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Evaluation of Assembly Simulators Used in Closed Loop Attitude
Control System Testing

by

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ABSTRACT

The Cassini spacecraft's Attitude and Articulation Control Subsystem has been tested extensively at the Jet Propulsion Laboratory in Pasadena, California. Three of the subsystem's assemblies have been tested using assembly simulators in place of actual hardware. These simulators have been designed and tested to ensure as much commonality with the hardware as possible. Several early design choice have impacted the degree to which the simulators have matched the hardware, the most crucial decision concerning the interface between the assembly simulators and the flight hardware. However, these difficulties were overcome and all testing requirements were satisfied.

The use of simulators has resulted in increased testing ability due to the small number of flight components constructed. Though this experience, several key lessons were learned, chief among them being clear definition of expectations and the importance of defining simulation interfaces as identical as possible to the flight equipment. Assembly simulators, properly developed, should prove a valuable alternative to physical hardware testing for future flight projects.

Thesis Advisor: Professor Steven R. Hall
Associate Professor of Aeronautics and Astronautics

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Acronym List

AACS	Attitude and Articulation Control Subsystem
ACC	A c c e l e r o m e t e r
AFC	AACS Flight Computer
ALF	Accelerated Load Format
ATLO	Assembly, Test and Launch Operations
BAIL	Backdoor ALF Injection Loader
BPLVD	Bi Propellant Latch Valve Driver
CATS	Cassini AACS Test Station
CDS	Command and Data Subsystem
DARTS	Dynamics Algorithms for Real Time Simulation
EFC	Engineering Flight Computer
EGA	Engine Gimbal Actuator
EGECU	Engine Gimbal Electronics Control Unit
EGED	Engine Gimbal Electronics Driver
GMT	Greenwich Mean Time
FSDS	Flight Software Development System
HELVD	Helium Latch Valve Driver
IRU	Inertial Reference Unit
ITL	Integration and Test Laboratory
JPL	Jet Propulsion Laboratory
MEVD	Main Engine Valve Driver
MPD	MonoPropellant Driver
Pcu	Power Conversion Unit
PIU	Pixel Input Unit
PMS	Propulsion Module Subsystem
Pou	Pixel Output Unit
PPS	Power and Pyrotechnic Subsystem
RWA	Reaction Wheel Assembly

RWM	Reaction Wheel Motor
RWX	Reaction Wheel Electronics
SEHW	Support Equipment Hardware
SESW	Support Equipment Software
SSH	Sun Sensor Head
SSE	Sun Sensor Electronics
SSPS	Solid State Power Switch
SRU	Stellar Reference Unit
VDECU	Valve Drive Electronics Control Unit
VDEX	Valve Drive Electronics Extension

Chapter 1

Introduction

In October 1997, a Titan IV/Centaur launch vehicle will lift the **Cassini** spacecraft towards Saturn, beginning the last in a series of grand tour missions that included the Voyager probes and the Galileo spacecraft. Cassini's mission is to deliver the **Huygens** Titan probe to the surface of Titan and to perform an orbital analysis of the **Saturnian** system. The spacecraft has been developed and tested primarily by the California Institute of Technology's Jet Propulsion Laboratory (**JPL**) for NASA's Office of Space Science.

The attitude and articulation control subsystem (**AACS**) for Cassini has been extensively tested at JPL through a comprehensive closed loop testing plan. The AACS has a number of inputs to allow for support equipment to simulate the outside environment of the spacecraft during the mission. Examples of these inputs include accelerometer and gyroscope biases, simulated starfields and simulated sun sensor inputs. Interfaces external to the AACS are also simulated. These include the Command and Data Subsystem (**CDS**), the Power and Pyrotechnic Subsystem (**PPS**) and the Propulsion Module Subsystem (**PMS**). This allows for the hardware to experience **flightlike** conditions (with the exception of environmental conditions) and makes closed loop testing possible.

However, in many cases it is not possible for a complete set of AACS hardware to undergo this extensive testing. During the busiest testing period, three laboratories are running simultaneously at JPL for AACS testing. For most of the hardware, there exists sufficient flight hardware to accommodate these laboratories. But for three assemblies, this is not the case. Due to the high cost of these assemblies and the quicker development time of simulators, the reaction wheel assembly, the inertial reference unit and the engine gimbal actuators are replaced by assembly simulators during closed loop testing.

These simulators play a pivotal role in AACS testing. During pre flight testing, the simulators must act sufficiently like the flight units to permit testing of software functionality and mission sequences. After launch, these simulators are even more important as they become the only mechanism by which testing of sequences or anomalies can occur.

This thesis evaluates the effectiveness of these simulators during testing of the AACS at JPL. With all of the laboratories relying on these simulators after launch, it is very **important** to understand the consequences of this approach. As the trend to drive down develop costs in space missions

continues, there is every reason to expect that future missions will have to rely on assembly simulators in an ever increasing capacity. Evaluation of these assemblies of the **Cassini** spacecraft is a step toward developing a knowledge base that could be used when considering different testing options in the future.

This thesis begins with a description of the closed loop testbed at JPL and how the laboratory environment works. This is followed by an analysis of the testing of the engine gimbal actuators, the inertial reference unit and the reaction wheel assembly. Finally, we conclude with an evaluation of the testbed as a whole as well as lessons learned during closed loop simulation.

Chapter 2

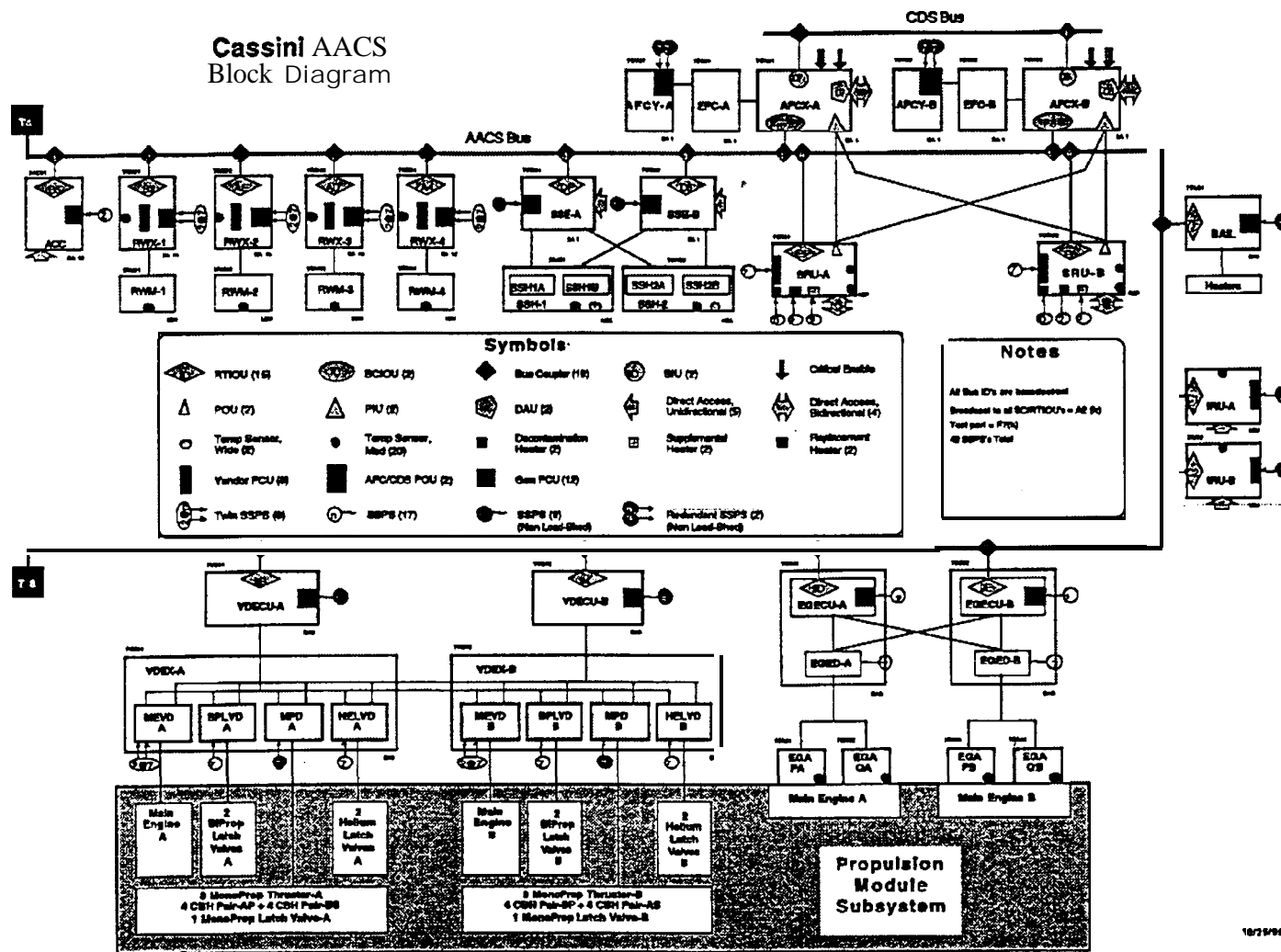
Closed Loop Attitude Control Testing

2.1 AACS

The attitude and articulation control subsystem is responsible for attitude determination and control during all phases of the mission. The components of the AACS are shown in figure 2.1 and are described briefly below.

- .AACS Flight Computer (AFC): The AFC is responsible for acting on commands from the command and data subsystem (CDS) concerning guidance, navigation and control. The system is dually redundant and interfaces with the AACS databus, the CDS databus and the power and pyrotechnic subsystem (PPS). The AFC direct access port is used to send commands to the AFC when the CDS is not present during test. The AFC also interfaces with the Stellar Reference Unit through a dedicated databus used to gather pixel information during Star Identification.
- .Accelerometer (ACC): The accelerometer is used to determine changes in velocity along the spacecraft Z axis. The accelerometer is a non redundant component that interfaces with the PPS and the AACS databus. The accelerometer has a direct access port that allows for simulation of Z axis acceleration during testing.
- .Backdoor ALF Injection Loader (BAIL): This assembly is a fault protection device that is used to provide a level of redundancy in the event that CDS has difficulty loading the AFC with its software. The BAIL contains accelerated load format (ALF) data blocks that can load the AFC in the event of problems with nominal loading via CDS.
- .Engine Gimbal Electronics/Actuators (EGE/EGA): The EGA's articulate the gimbals attached to the dual main engines of the spacecraft. The EGA's are controlled by the EGEs, which interface with the AACS databus.
- .Inertial Reference Unit (IRU): The dual redundant IRU uses a set of four hemispherical resonating gyros (HRG) to provide inertial rate information to the AFC for use in attitude control.
- .Reaction Wheel Assembly (RWA): There are four RWA's on the spacecraft. Three of these are arranged for use as actuators during attitude control. The fourth wheel is redundant and can be positioned to replace any of the three primary wheels in the event of a failure.
- .Stellar Reference Unit (SRU): The dual redundant SRU is a sensor used to determine position

Figure 2-1 Attitude and Articulation Control Subsystem Block Diagram



and attitude during the cruise portion of Cassini's mission. It utilizes a charged coupled device (CCD) camera to detect bright bodies in its field of view and this data is passed to the AFC via a pixel interface unit (PIU) for processing.

.Sun Sensor Assembly (SSA): The **dual** redundant sun sensor assembly is used to detect the position of the sun during attitude determination. Sun sensor heads are placed on the high gain antenna and generate voltages proportional to the amount of light that hits the heads.

.Valve Drive Electronics (VDE): The valve drive electronics are used to interface with the Propulsion Module Subsystem to open and close the various thrusters used for attitude control and as well as the main engine valves.

2.2 AACS Closed Loop Testbeds

2.2.1 ITL

The primary lab for integration and test of the AACS at the subsystem level is the Integration and Test Laboratory (ITL). The purpose of the ITL is to perform hardware integrations of the AACS subsystem and test functional sequences of the Cassini mission. All flight hardware as well as engineering models or flight spares are tested in the ITL to ensure proper electrical configuration when the assembly is integrated with the AACS databus, the Power and Pyrotechnic Subsystem (PPS) and the Propulsion Module Subsystem, if applicable (VDE, EGE/EGA). For this purpose, there are hardware simulators of the PPS and PMS in the ITL that allow testing of the interfaces to these subsystems.

For testing functional sequences, the ITL has an extensive set of support equipment hardware and software. The hardware and software work together to simulate the external interfaces to the AACS and permits closed loop testing. Support equipment hardware consists of a series of computers and additional equipment which interface with the users of the system as well as the hardware. This equipment includes an Inertial Sensors Controller (INS Controller) that permits biasing of the accelerometer and inertial reference unit, the assembly simulator hardware for the engine gimbal actuators, the inertial reference unit and the reaction wheel assembly, electronics to generate bias voltages to send to the sun sensor assembly and star field data to send to the stellar reference unit, and equipment to interface with the AACS Flight Computer. The hardware also includes the simulators for the command and data subsystem, the PPS and the PMS.[2]

Support equipment software is an extensive network of computer programs working to simulate

the outside environment of the spacecraft. The programs fall into two large groups-- real time and non real time. Real time programs consist of the assembly simulator software, subsystem simulation software (e.g. CDS, PPS, PMS), as well as software to monitor different assemblies and report on their status. The non-real time software includes tasks such as user console interfacing and generation of displays.

The software also uses the concept of a “blackboard” to provide for data visibility across the simulation. The software runs on a set of five processors called chassis. These processors must work in a synchronized fashion and timing is very critical. Therefore, the processors use shared memory to facilitate data transfer. All of the chassis use the same set of memory to read and write variables. This means that all of the processors know what the state of the system is at any given time. This is analogous to how a common blackboard is used so that all those in a room have a consistent data set, and thus this reflective memory is known as the blackboard. [4]

Finally, the dynamics of the simulation are propagated in real time via a computer program called DARTS- Dynamic Algorithms for Real Time Simulation. This program was developed by A. Jain of the Jet Propulsion Laboratory and computes the time rate of change of the state of the Cassini spacecraft as a dynamical system[3]. The program accepts any number of actuators, sensors and flexible modes and thus is what makes closed loop dynamics testing possible for Cassini.

The ITL also permits some level of system mode testing. The Command and Data Subsystem is usually simulated in the ITL, but for some testing, the actual CDS is used and the AACS Flight computer takes its commands from the actual command computer. This permits testing of the CDS-AACS interface in the ITL before assembly, test and launch operations begin.

2.2.2 Cassini AACS Test Station

There also exists the Cassini AACS Test Station (CATS) for development of flight and support software. CATS is similar to the ITL in that actual hardware is present in most cases, support equipment hardware processors are used to interface with the hardware and users, and a closed loop dynamics environment is possible with the use of DARTS. The major difference between CATS and ITL is their purpose. ITL is used to test electrical interfaces of the flight hardware and thus all hardware that is flight certified is first tested in the ITL before delivery to the Spacecraft Assembly Facility. CATS, on the other hand, is used to test the software of the system. The hardware is

present, but electrical “breadboards” are primarily used in CATS. The functionality of these breadboards is identical to the flight units in most cases, but shielding, grounding and electrical interfaces may be different.

2.2.3 Assembly, Test and Launch Operations

Assembly, Test and Launch Operations (ATLO) for Cassini began in late 1995 and will continue through launch of Cassini in October, 1997. Primarily testing occurs at the Spacecraft Assembly Facility at JPL. At this location, the flight hardware is integrated together for the final time. Also, many of the simulators are not present. The PPS hardware is there, and thus all power comes from the actual PPS. There are no assembly simulators once all the hardware is integrated. The CDS is also present and there is no CDS simulator. However, there is one simulator still present, The PMS simulation is still running in ATLO due to the danger to personnel of testing main engine firings and reaction control thrusters. The Propulsion Module is tested separately by Lockheed Martin for the vast majority of the testing period. During most testing in ATLO, the DARTS simulation is still present and permits closed loop testing. The exception is during environmental testing when the support equipment is disconnected and no closed loop testing is conducted.

Throughout the testing plan, the EGAs, RWAS and IRUs are simulated in the ITL and in CATS. The real hardware is present for interface checkout in the ITL and during ATLO testing. The next sections go into detail concerning the three assembly simulators and evaluates their usage in the testing of Cassini’s AACS.

Chapter 3

Engine Gimbal Actuators

3.1 Description

The purpose of the engine gimbal actuators is to rotate the main engines of the propulsion module subsystem about their gimbal axes in response to commands by the AACS flight computer. The main engines are rotated such that the thrust vector-passes through the center of mass of the spacecraft as well as in the desired inertial direction. The IRU and ACC are used in conjunction with the EGA's to determine this direction as well as to determine when the required velocity change has been achieved.

A signal flow for the EGA's is shown in figure 3.1. The actuators act on extension commands pro-

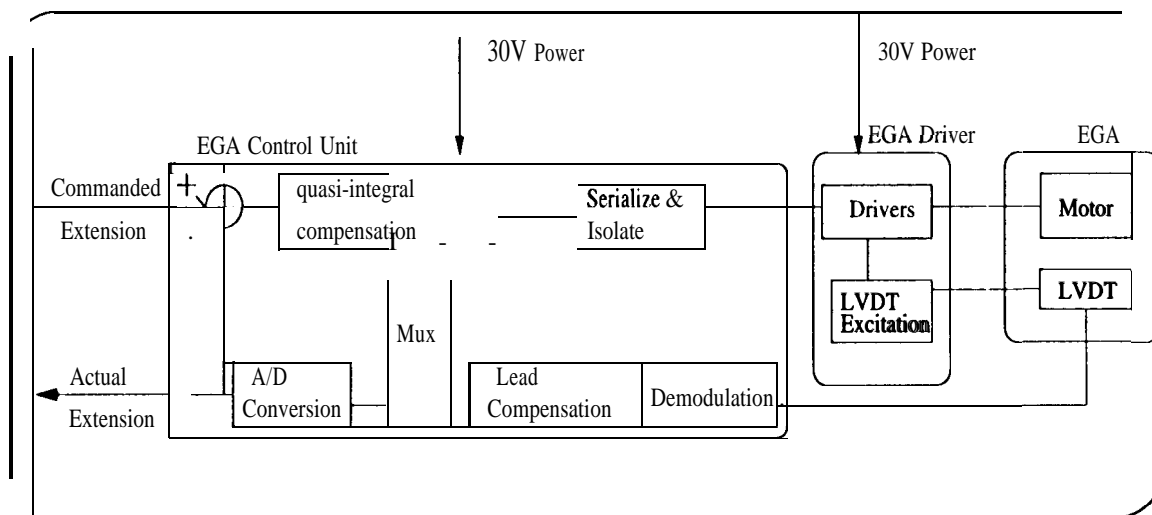


Figure 3-1 Engine Gimbal Actuator Block Diagram

vided by the AACS flight computer through the engine gimbal electronics. The extension is controlled by comparing the actual positions of the actuators to the desired position and correcting the position by altering the motor voltage. The actual positions are determined by the feedback signal from a Linear Variable Differential Transformer (LVDT) that is attached to each actuator. The electronics that control the position consist of a control unit and a driver. The driver accepts voltage commands from the control unit and generates excitation signals for the motor and the LVDT of the actuator. The control unit accepts commanded extensions off the AACS databus and the

LVDT feedback signal. The control unit generates a digital representation of the LVDT signal for the databus as well as the voltage commands for the driver.

3.2 Cassini Laboratory Configuration

The Engine Gimbal Actuators are simulated in the ITL and CATS through a combination of a hardware simulator and a software dynamics interface. The purpose of the hardware is to simulate the engine gimbal actuators and generate a feedback **signal** that represents the LVDT signal for the real actuators. The dynamics software accepts the commanded extensions and the LVDT extension information and then computes the main engine thrust vector direction for use in the DARTS simulation.

3.2.1 EGA Hardware Simulator

Description

The EGE hardware simulator was designed to simulate the LVDT feedback information that is supplied by the real EGAs in response to the LVDT excitation signal and the motor drive input. A block diagram is shown in figure 3.2.

To simulate the LVDT, the EGA hardware simulator consists of a motor simulator and the LVDT simulator. The motor simulator accepts the EGE drive signal and passes it through an optical isolator. The signal is scaled such that a position signal is generated that is proportional to the commanded position of the actuator. Then, this signal is multiplied by the LVDT excitation signal, also received from the EGE. The multiplication retains the sign of the motor drive signal and the result thus simulates the LVDT feedback signal.

Validation Test

When the engine gimbal actuators are integrated into the subsystem in the ITL, they are integrated per a hardware integration procedure. This procedure exercises the actuators and ensures that they perform adequately. Since the simulators and the real actuators are integrated using the same pro-

cedure, the data can be compared to evaluate the simulators.

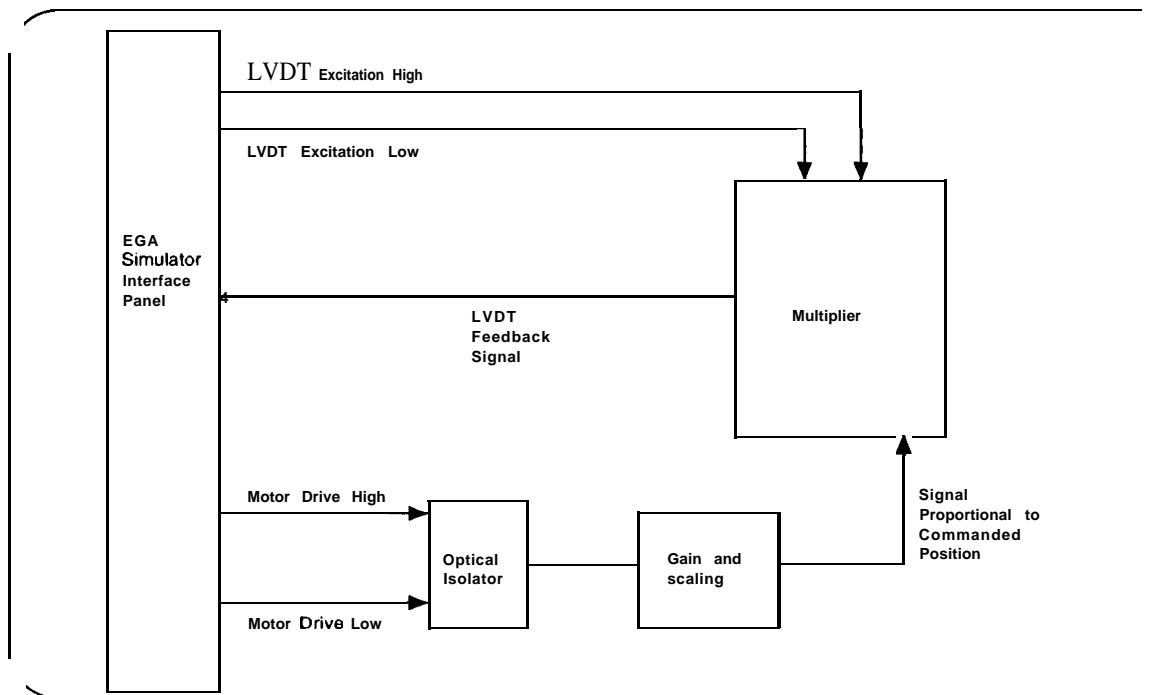


Figure 3-2 Engine Gimbal Actuator Hardware Simulator

The actuators (or simulators) are exercised through a series of extensions during the integration procedure. The results of this procedure was that the simulators perform to within specified tolerances and track the hardware very well and these results are summarized below:

.Average absolute deviation from the commanded position for simulation serial number 005 was 0.0326 mm.

.Average absolute deviation from the commanded position for simulation serial number 010 is was 0.0215 mm.

.Cassini AACS requirement: O. 1 mm deviation.

Even though the AACS requirement was met on average, the maximum error did deviate from the AACS requirement for both of the simulators. This deviation was deemed acceptable for testing, however. This is because Cassini fault protection will activate if the deviation is greater than 0.27 mm for two consecutive readings of the EGA (reading occur every 125 ins). This behavior was not observed when testing either the EGA's or the EGA simulators and thus the EGA simulators were accepted for testing. Due to the variance of the EGA positions, the power measurements of

the EGAs also had more variance than with the flight equipment, but this was also acceptable. [5]

Differences and Problems

One problem that did occur during testing is that a fault protection error in flight software was not found in the ITL testing and the bug was discovered when the fault protection autonomously powered down the EGA driver during integration of the flight Propulsion Module Subsystem on the actual spacecraft. The investigation concluded that the EGA simulators were not designed to simulate an EGA under actual flight loading conditions. Therefore, the first time the flight software interfaced with an EGA loaded onto a gimbal and a Main Engine was during ATLO testing. This brought out one of the important lessons learned through AACS testing. If the requirements are not stated clearly at the outset and thought through in their entirety, unforeseen events may occur. The result of this testing in ALTO was a decision to use flight spare EGAs attached to a load fixture for future testing. Thus the EGA simulators will not be used for post launch ITL analysis activities.

3.2.2 EGA Dynamics Model

Description

To properly represent the motion of the EGA's in the closed loop dynamics simulation, the support equipment software must ensure that the main engine thrust vector direction is consistent with the EGA extensions. To accomplish this, a software "model" of the EGA accepts information from the EGA (or EGA simulator) and computes the main engine thrust vector. The relationship be-

tween the EGA (or simulator) and the EGA “model” is shown in figure 3.3 and is described below.

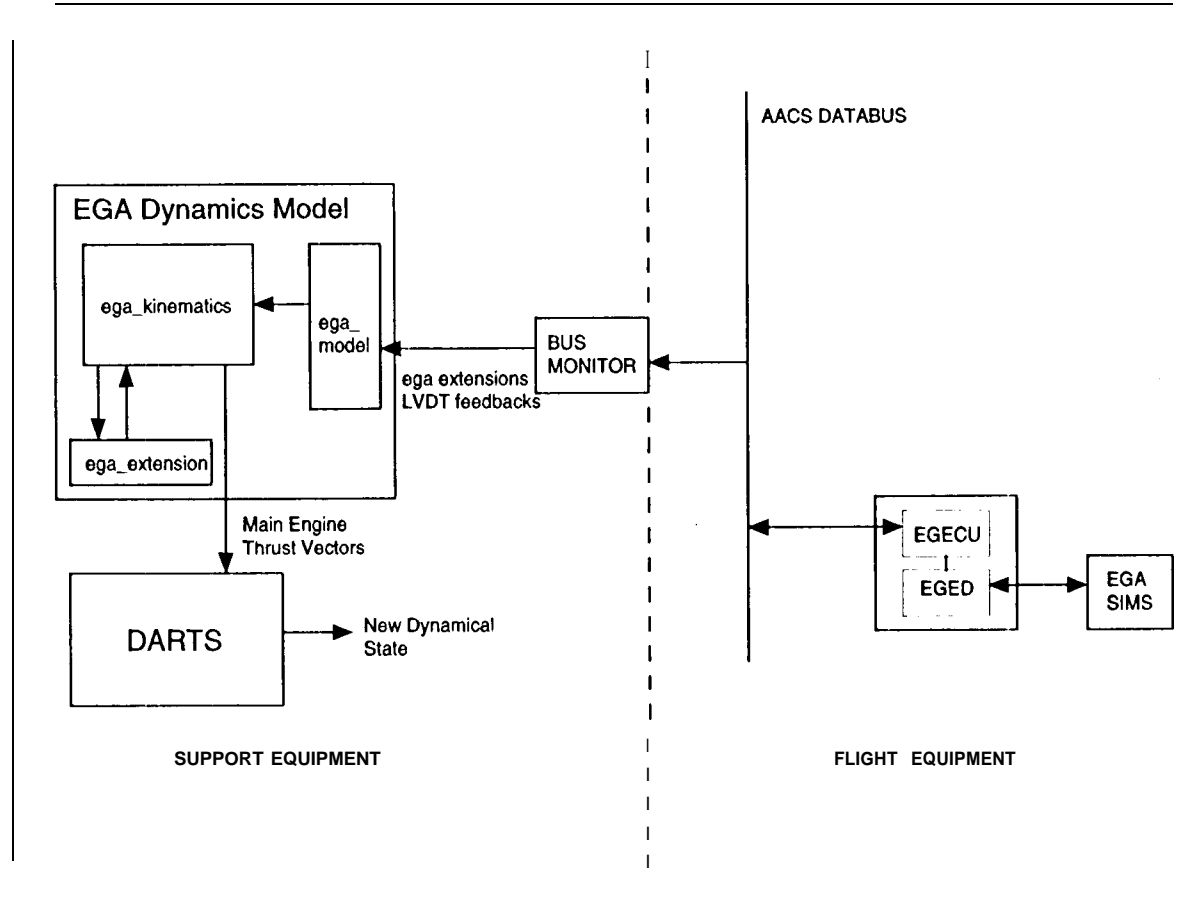


Figure 3-3 Engine Gimbal Actuator Dynamics Model

The model consists of three modules: `ega_model`, `ega_kinematics` and `ega_extension`. The first module, `ega_model`, accepts the LVDT and commanded extension information and computes the new extensions of the actuators. This is done without regard to dynamics and the extension is simply set to the current commanded extension. The only exception is if the step required to update the position is too high. In this case, the model updates the extension with a series of smaller steps. Once the extensions are computed, `ega_kinematics` is called. This module calculates the thrust vector by first computing the gimbal angles (accomplished by the module `ega_extension`) and then transforming the angle information into the main engine thrust vector direction. Once the thrust vector direction is known, this information is used during the next iteration of the dynamics simulation.

Validation Testing and Results

The EGA model was validated by comparing resulting engine gimbal angles to analytical predicts. The EGAs were commanded to several different positions and the computed main engine thrust vector was recorded. Given this thrust vector, a solution for the EGA position was derived and compared to the commanded position. The data was consistent and the model was validated in this isolated case. The table below shows the predicted and actual values for the EGA extensions in response to several command to stroke the gimbal actuators.

'E-GA P Commanded	EGAP Actual	EGA Q Commanded	EGA Q Actual
0	0	19	18
1563	1563	0	0
1563	1563	1563	1563
-155	-155	1563	1564
-155	-155	961	962
-963	-963	961	962
-963	-963	-1563	-1562
155	155	-1563	-1562
155	155	-961	-960
0	0	-961	-960
0	0	-1	0
960	962	-1	1
960	962	-960	-961
-1563	-1562	-960	-959
-1563	-1563	-1563	-1562
-962	-962	-1563	-1562
1563	1563	961	961
1563	1563	1563	1563
0	0	1563	1564
0	0	0	1

3.2.3 Closed Loop Simulation

The two primary test activities of the laboratory that have validated the described EGA simulation have been the Main Engine Trajectory Correction Maneuver (TCM) Testing and Fault Injection

Testing. The purpose of the Main Engine TCM is to test the hardware and software under a realistic set of circumstances where the main engine is used to alter the path of the spacecraft, Precision Thrust Vector Control (TVC) is performed by the flight software and it is critical that the dynamic model of the actuators alter the thrust vector as commanded by the flight software. As the following data in figures 3.4 and 3.5 shows, the EGA simulators performed well in a closed loop environment. The X and Y components of the thrust vectors of the simulation(py_me_0 and

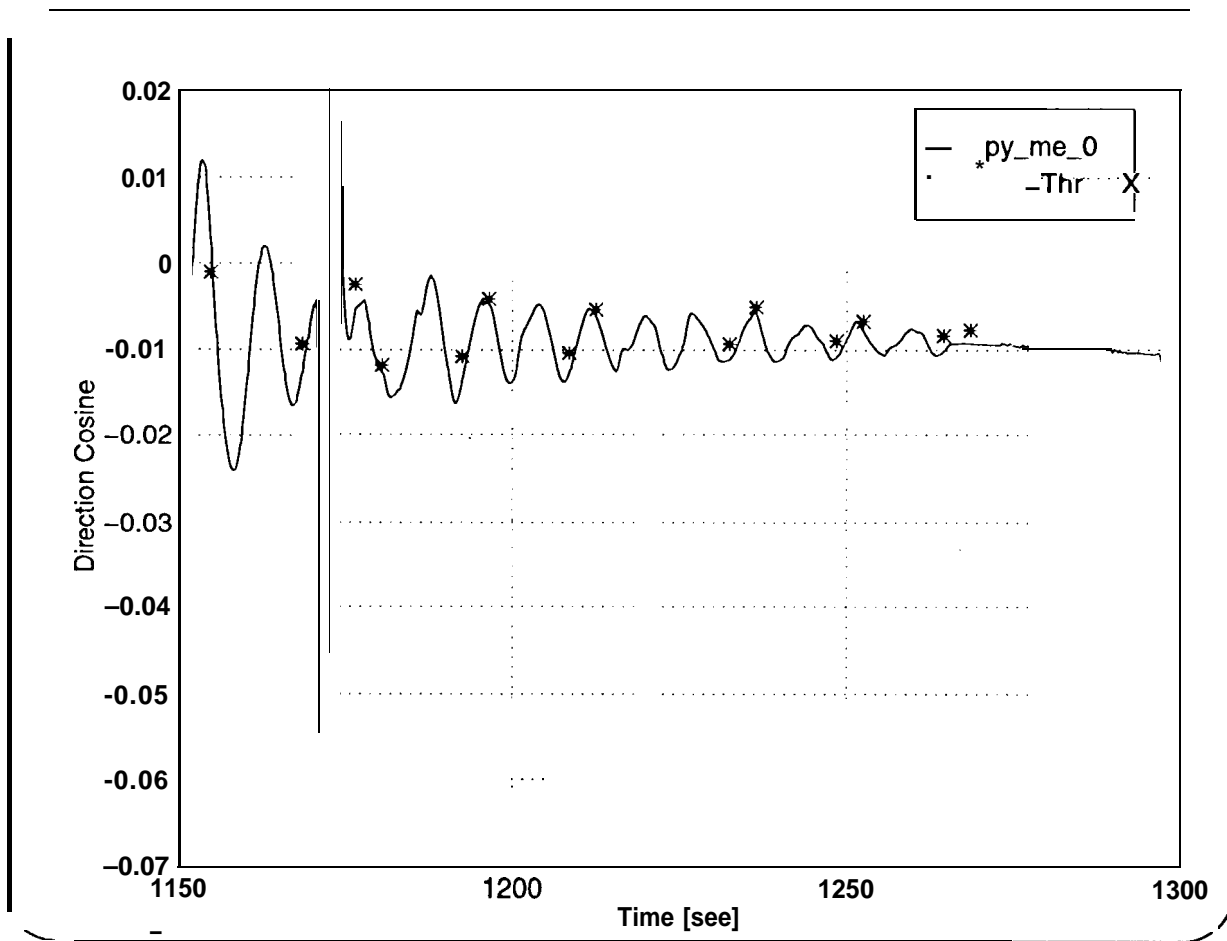


Figure 3-4 Simulated and Flight Software Thrust Vectors in the X direction

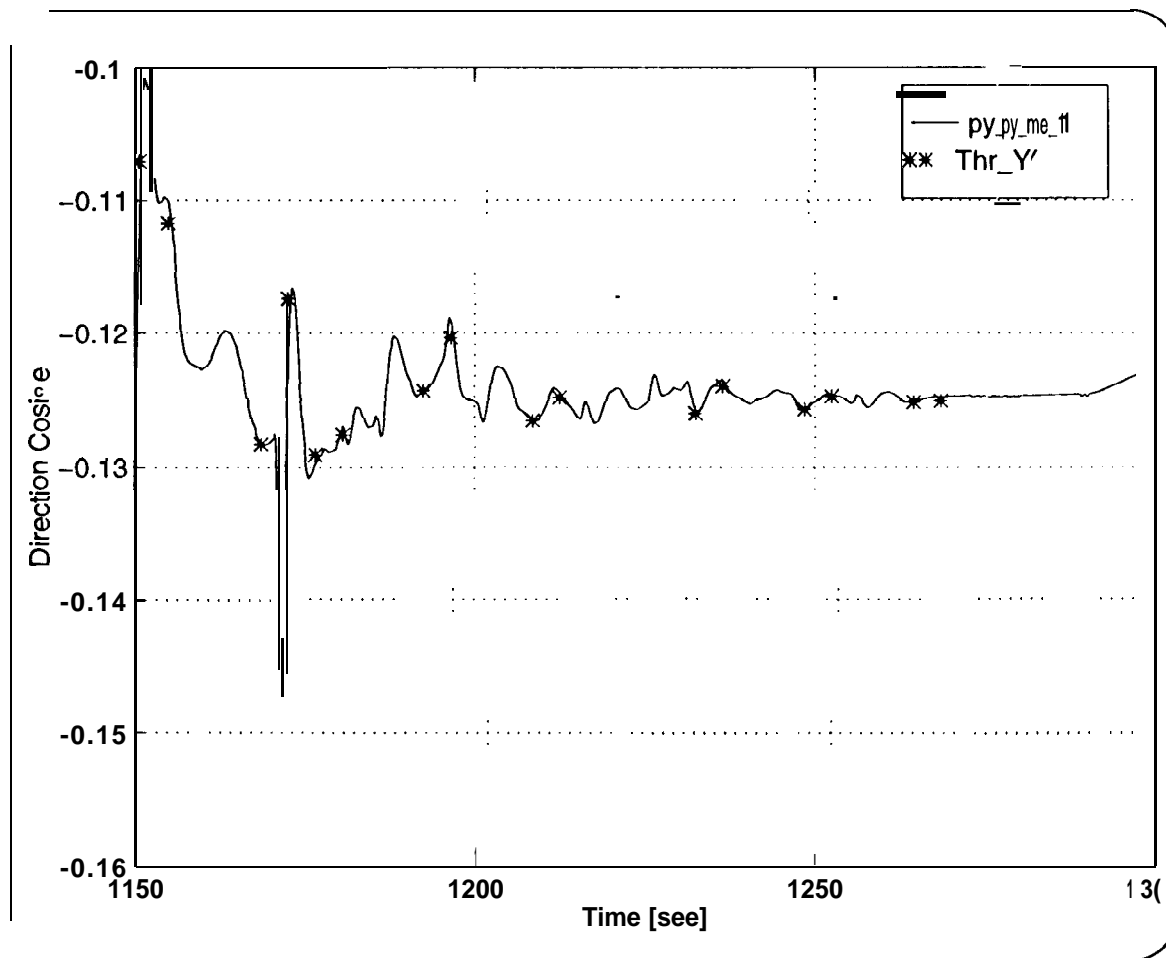


Figure 3-5 Simulated and Flight Software Thrust Vectors in the Y direction

1]) and what flight software believed to be the thrust vector (Thr_[X and Y]) matched very well. A Z component comparison is not available since the flight software does not record Z axis data since the direction cosine is so close to one.

Another closed loop aspect of the EGA simulation is the task of injecting faults into the simulation to test the fault protection responses. The EGA simulator was designed to interface with the support equipment exactly like the real hardware. Thus, it was not possible to simulate any faults that involved hardware failure. The software dynamics model could have been altered to simulate many faults, but since there is no way to **alter** the EGA hardware simulator there was no need. If the model was to simulate a stall, for example, it could easily be disabled from the rest of the simulation. This would not be possible for the hardware, however, and the result would be flight software receiving an external disturbance with no indication that a stalled EGA is the cause.

3.3 Evaluation

The EGA simulation met the requirement for test of the engine gimbal electronics. Specifically, the EGA simulator did not cause fault protection to activate unexpectedly during testing in either CATS or ITL. This facilitated testing of the flight software, as well as the Main Engine Trajectory Correction Maneuver. Due to the nature of the hardware simulator, testing of the fault protection capabilities was not performed. When the flight actuators were integrated with the AACS and the flight PMS, fault protection did activate unexpectedly. But since the EGA simulators were never meant to simulate a loaded EGA, the conclusion is that the EGA simulator did perform adequately during AACS testing.

Chapter 4

Inertial Reference Unit

4.1 Description

The Inertial Reference Unit (IRU) is a dual redundant assembly that is used to detect inertial angular velocity of the spacecraft. Each IRU contains four hemispherical resonating gyroscopes and processing electronics. The IRU contains its own processing circuitry that interfaces with the AACS databus RTIOU and the gyroscopes. A block diagram of the IRU is shown in figure 4. 1.[6]

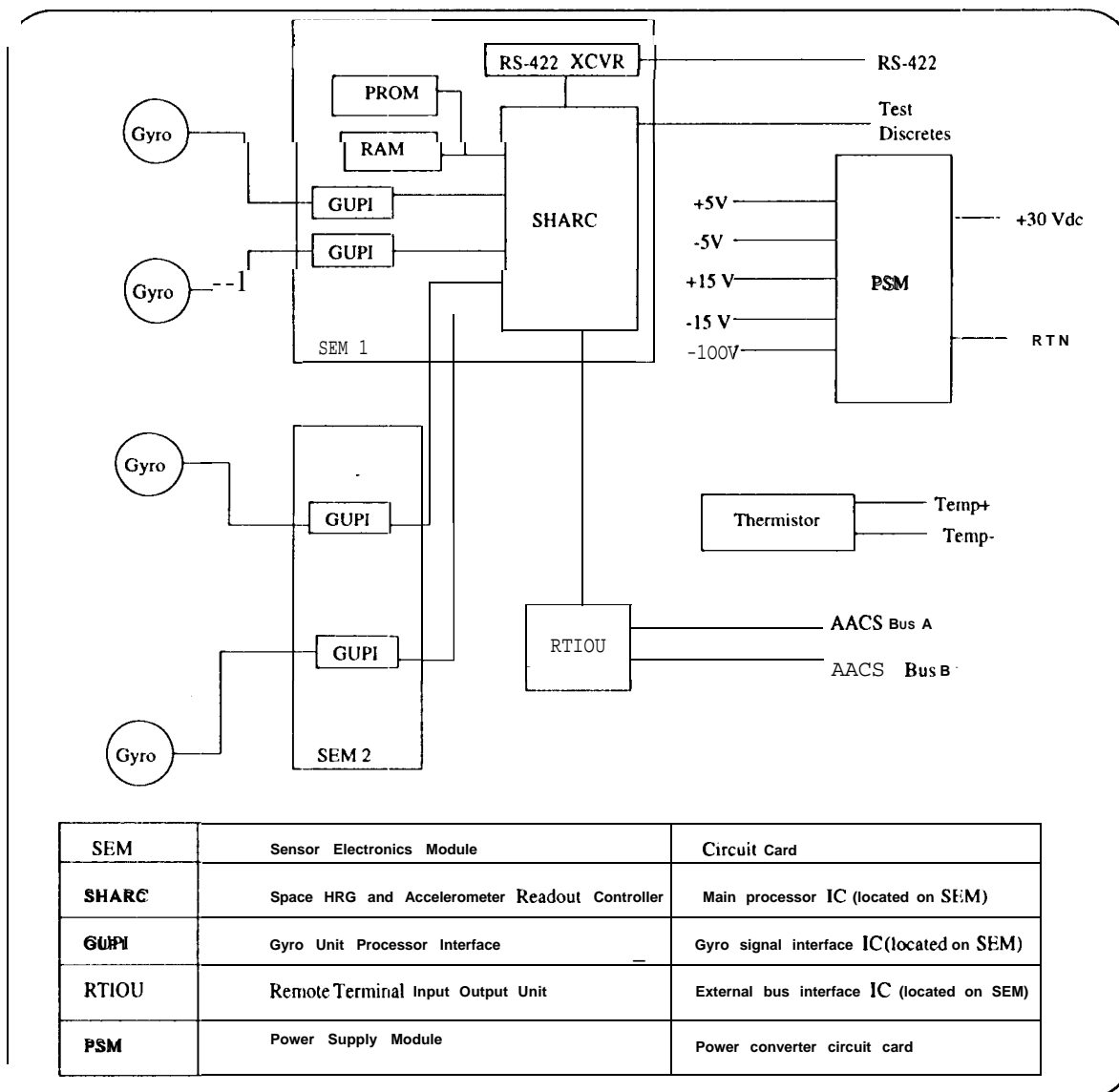


Figure 4-1 Inertial Reference Unit Block Diagram

The gyroscopes each run at a frequency of approximately 2000 Hz and a rate estimate is obtained from the gyroscope every cycle. The SHARC processor has software that runs at 100 Hz. Each time the software loop is executed, the rate measurements since the last time the software was executed are integrated and the angle is added to the data that will be passed to the flight computer. The flight computer can read the accumulated angle or the IRU status from the IRU. The AFC can also write data to the IRU. This data, for example, would be new software to the SHARC in the event of an IRU reset.

4.2 Cassini Laboratory Configuration

As in the case with the EGA simulation, there are two parts to the IRU simulation- an assembly simulator and a dynamics model. The assembly simulator is software that represents the IRU when the actual hardware is unavailable in the laboratory. The dynamics model is used to generate biases for the IRU by converting the spacecraft angular rates to rates in the gyro sensing axes which are used to bias either the real gyros or the simulator.

4.2.1 IRU Assembly Simulator

Description

The assembly simulator has the function of accepting biases from the dynamics interface and converting these biases into data for the flight software to interpret. This simulator consists of three parts. The first is a remote terminal input output unit. This unit is a remote terminal on the Cassini AACS databus and facilitates communication with the AACS flight computer. The second component is an interface card that communicates with the RTIOU. This card is a series of static RAM registers that the simulator can write to. This allows the software to act as the actual hardware by interfacing with the RTIOU similar to the actual hardware. The third component is the actual software for the IRU simulator. The software supports five functions of the IRU: power on initialization of the IRU output data, IRU Built in Test (BIT), IRU SHARC software download, IRU “soft reset”, and normal operation of the IRU. The data flow through these five functions are shown in

figure 4.2.

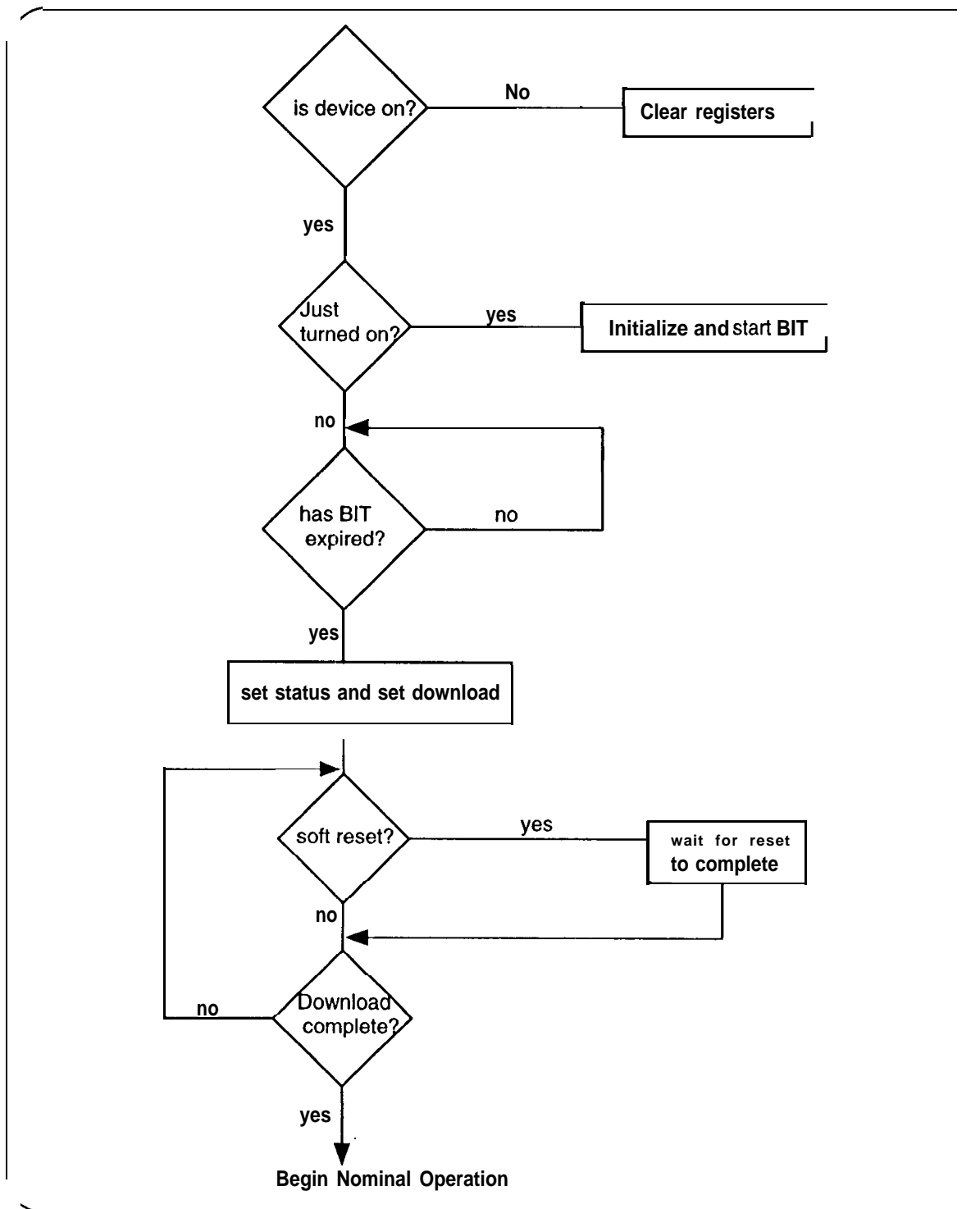


Figure 4-2 IRU Assembly Simulator Flow Diagram

Upon receipt of a power on command, the simulator sets all output information to zero and sets a timer to begin the BIT. The BIT simulation is a one second hold that simulates the time for the SHARC built in test. Once this hold is complete, the IRU simulator reports this information via the RTIOU to the flight software and sets a flag indicating readiness to begin the software download. The software download function is simulated by verifying receipt of the data sent by the flight software and then indicating a valid checksum and a valid load. The soft reset is another one second hold for the simulator and results in reporting a good status message back to the flight software after completion of the hold.

Finally, there is the actual operation of the IRU. The software checks for a soft reset and if none occurs, the software proceeds to calculate the outputs of the gyroscopes. Since the IRU simulator receives the rates the gyroscopes sense in the gyroscope coordinate system, the simulator simply has to convert these rates into a change in angle and properly format this information for the RTIOU. This is accomplished by multiplying the rate received by the IRU cycle time and adding this angle to the last angle computed to determine the accumulated angle. Once this is accomplished, the angle is converted to a form compatible with the RTIOU and the data is passed to the flight software.

Validation Testing and Results

This simulator was integrated into the ITL and CATS with the same integration procedure that was used for the actual flight hardware. Thus, we have a common test to compare the simulator and the hardware with. During the integration procedure, the gyros are biased with a set of support

equipment commands. Figures 4.3 and 4.4 show the result of these commands.

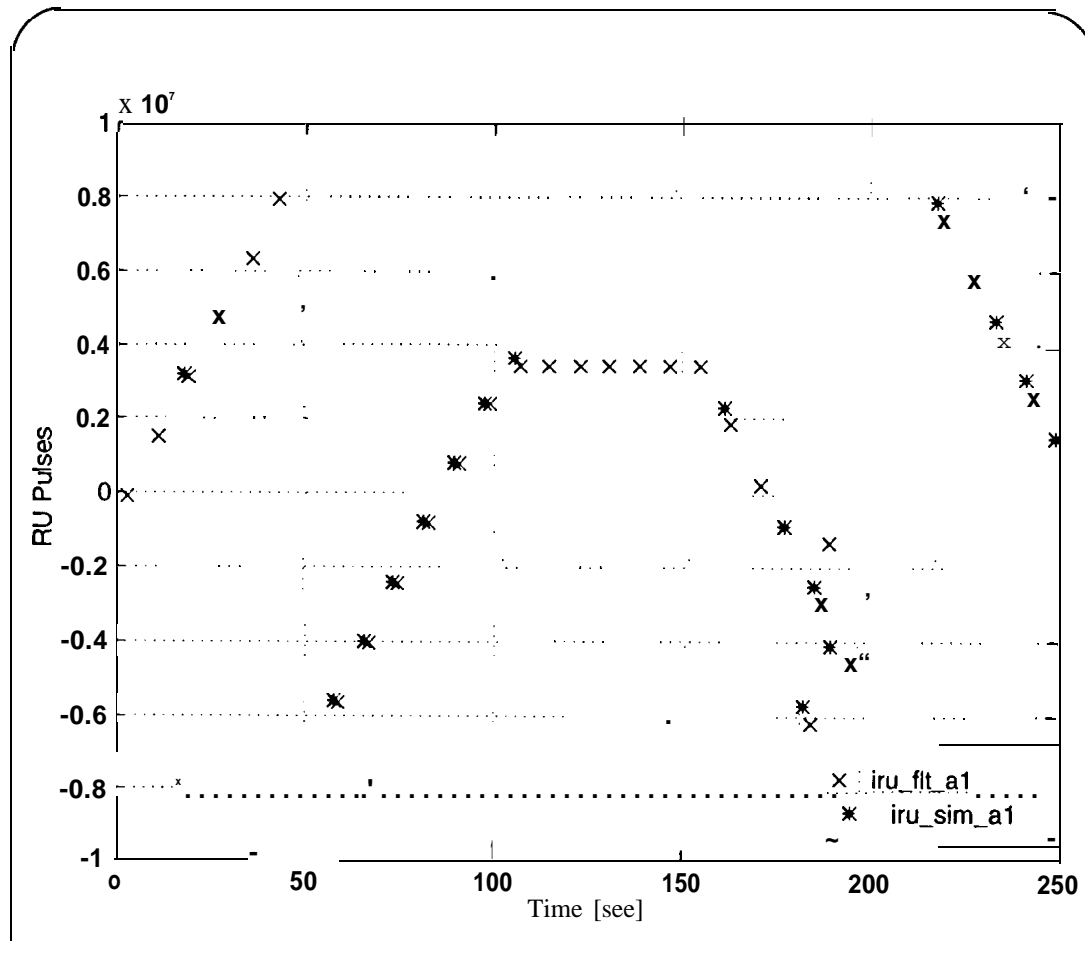


Figure 4-3 IRU Simulator and Hardware Comparison

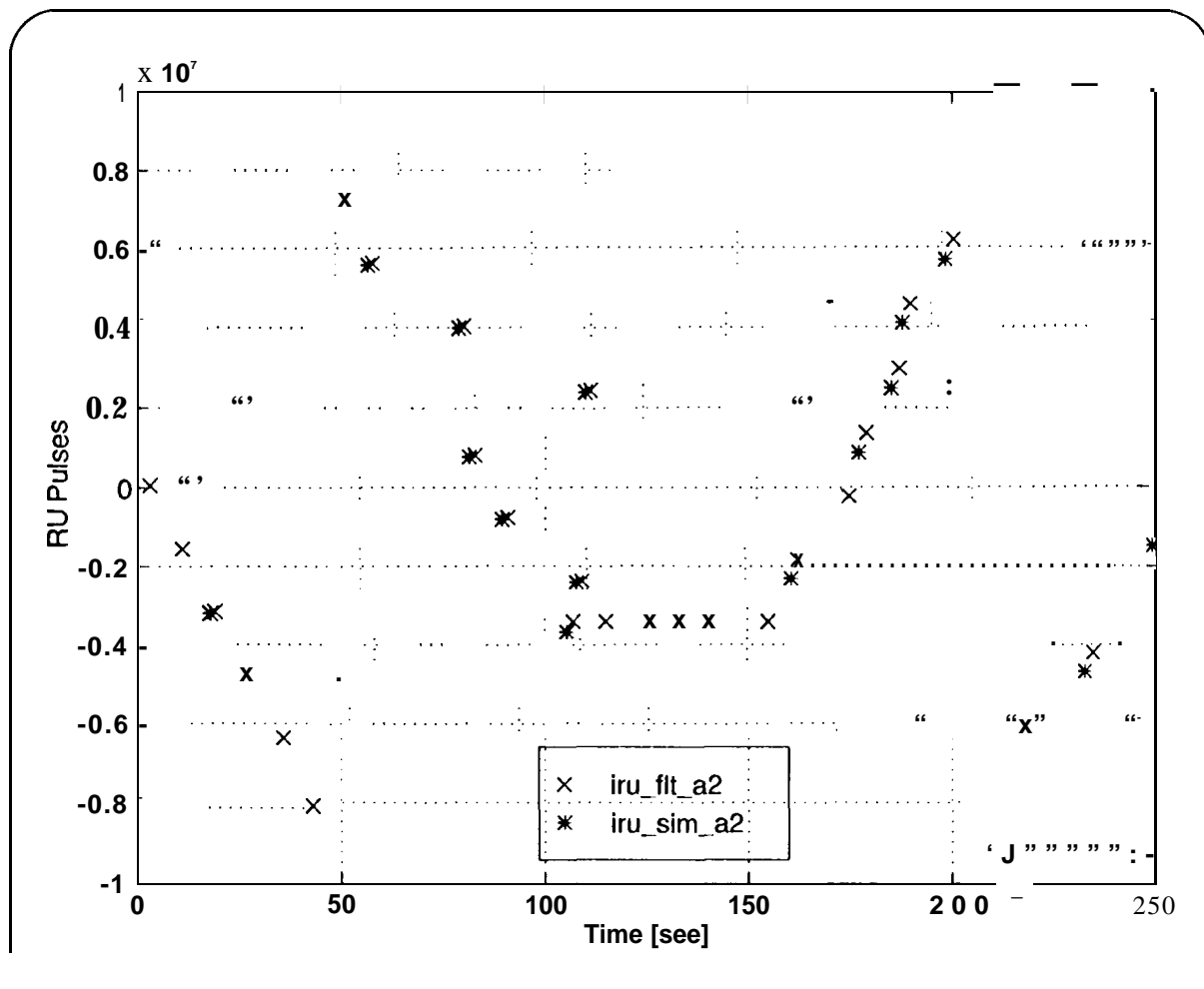


Figure 4-4 IRU Simulator and Hardware Comparison

As the data shows, the IRU simulators matched the performance of the flight equipment very well.

Differences and Problems

Integration revealed some problems with the simulator that have been corrected to increase the fidelity of the software. The first problem was with the processing cycle. The original version of the software integrated at the same speed as the dynamic simulation, 16 Hz. This is not consistent with the actual hardware, which reads data from all four gyros at a speed of 100 Hz. There is the danger that the simulator was running too slow and unrealistically large changes in angles would be reported by the simulator. It would be more consistent with the hardware if the software ran at a speed of 400 Hz and processed one gyroscope at a time. When all four gyros were processed, the simulator made this data available to the flight software through the RTIOU. This configura-

tion change was implemented and performs very well.

A second problem was with the noise of the IRU. The original model did not have any simulation of gyroscope noise and once again a change would improve fidelity. The final solution was for the model to cycle through a large set of experimental data representing realistic numbers for gyroscope noise. These numbers would be added to the output of the gyroscope and would simulate noise coming from the IRU gyroscopes,

A final problem was with the timing of the simulator. In reality, the IRU has a double buffer that is used to prevent the flight software from reading partially updated data. One of these buffers always has a complete packet of information for the flight software. However, the assembly simulator card does not support double buffering. Thus, flight software was reading the information out of the IRU simulator, but the information was not completely updated. To correct this problem, the assembly simulator card was modified such that when flight software was reading the information from the card, a signal was sent to the IRU assembly simulator. The software was changed to verify this signal was not active before a read was attempted. If this signal was sensed, output was delayed until the read was concluded. This correction worked very well and the information to the flight software was valid.

The general conclusion is that once coding errors are corrected, the simulator does act sufficiently like the hardware to permit testing. However, there are several aspects of the hardware that are not simulated. Essentially, the actual computation of the SHARC is not simulated. The Built In Test is not actually performed. Instead, a timer simulates the delay the BIT would cause in the processing cycle. Similarly, the checksum during the download of the new SHARC software is not performed. Again, a timer is used to simulate the delay of the download and checksum. This was done because simulation of the actual SHARC software was not an objective in the IRU simulation. The basic philosophy was that the inputs and outputs of the IRU would be as identical as the software team could make them to the hardware. Thus the simulator can report that the data has been received or that a BIT has been performed, but the BIT or data download may not have actually happened in the simulation software. This black box concept has important consequences when fault injection is considered.

One of the advantages of using simulators is that the test analyst has the ability to simulate faults without damaging actual hardware. However, with the IRU simulator, any faults to the SHARC or other processing electronics cannot be simulated. The simulators were designed such that the

“outside world” only “has a command path to the simulator if it has a command path to the actual device. Therefore, since one cannot command a BIT failure with the actual hardware, for example, it was decided that one would not be able to with the simulators either. Any fault injection would have to be possible with either real hardware or simulators and thus involve changing existing inputs into the devices. For example, it was possible to simulate a failed gyro by sending a large bias into one of the gyros. The **SHARC** or IRU simulator would see this large rate on one of the gyros and declare that gyro’s data invalid. But failures internal to the IRU would have to be simulated on another testbed.

4.2.2 Gyro Dynamics Model

The gyro model within the dynamics simulation computes the biases that are sent to the IRU assembly simulator model. The model is straightforward. First, the locations of the gyroscopes and the transformations of the angular rates of the spacecraft from spacecraft to the gyro sensing axes were determined and loaded into the model. Then the model accepts the spacecraft angular rates from the DARTS simulation and converts these to rates that the gyroscopes sense. Then this information is passed to the IRU model as described above, The interaction between the model and

the simulation is shown in figure 4.5.

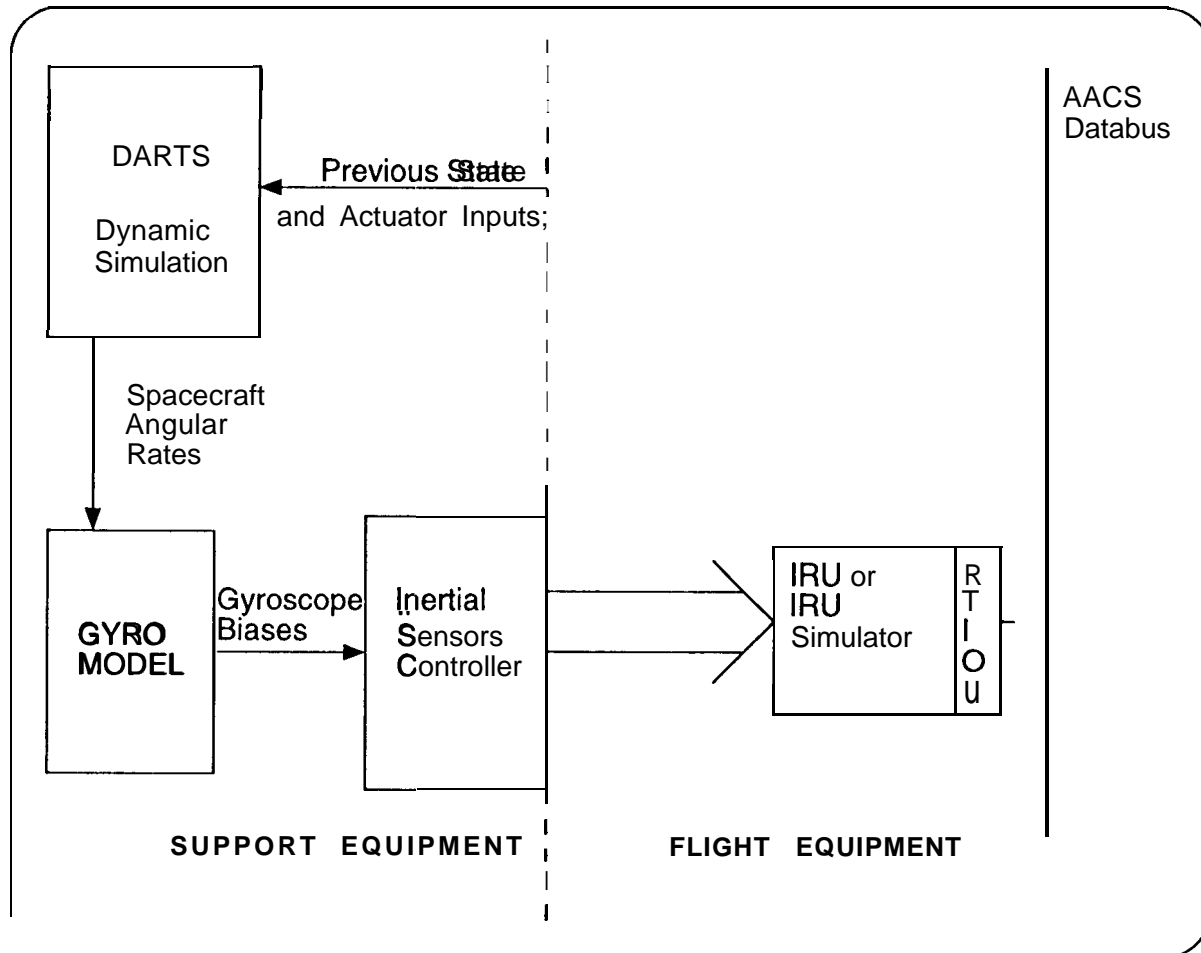


Figure 4-5 Inertial Reference Unit Dynamics Model

The gyroscope dynamics model was validated as a part of the closed loop simulation described below.

4.2.3 Closed Loop Simulation

The inertial reference unit simulator was used extensively in all laboratories during the testing of the Cassini AACSD. The criterion for success of the simulator is how effectively the simulated angular rates of the dynamics simulation are reported to the flight software. This can be shown by examining the reported spacecraft rate and the simulated rate. This is shown in figures 4.6 through

4.8. the variable “b_ang_rt_[x,y or z]” is the angular rate being simulated and the variable “[X,Y

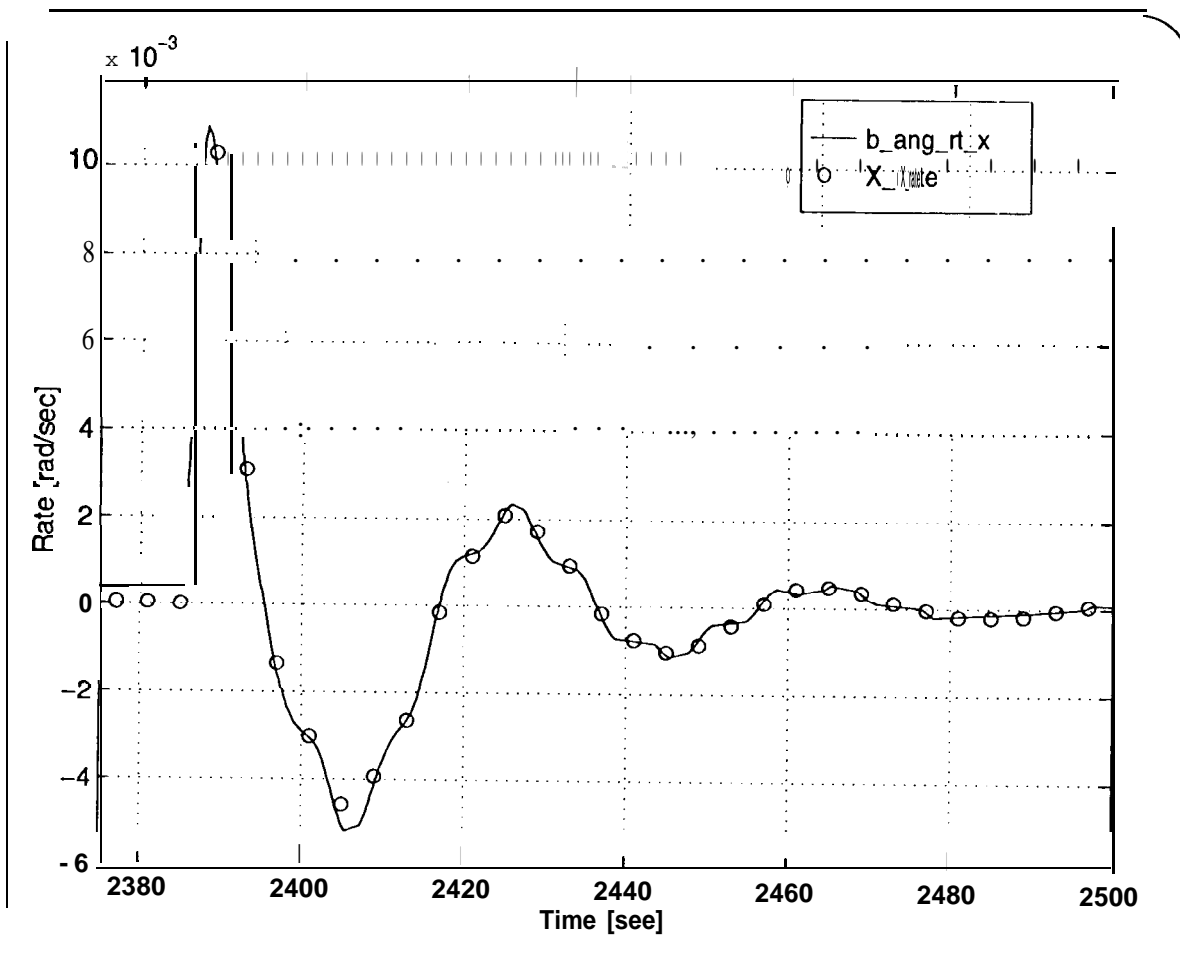


Figure 4-6 Simulated and Flight Software Angular Rates, X Axis

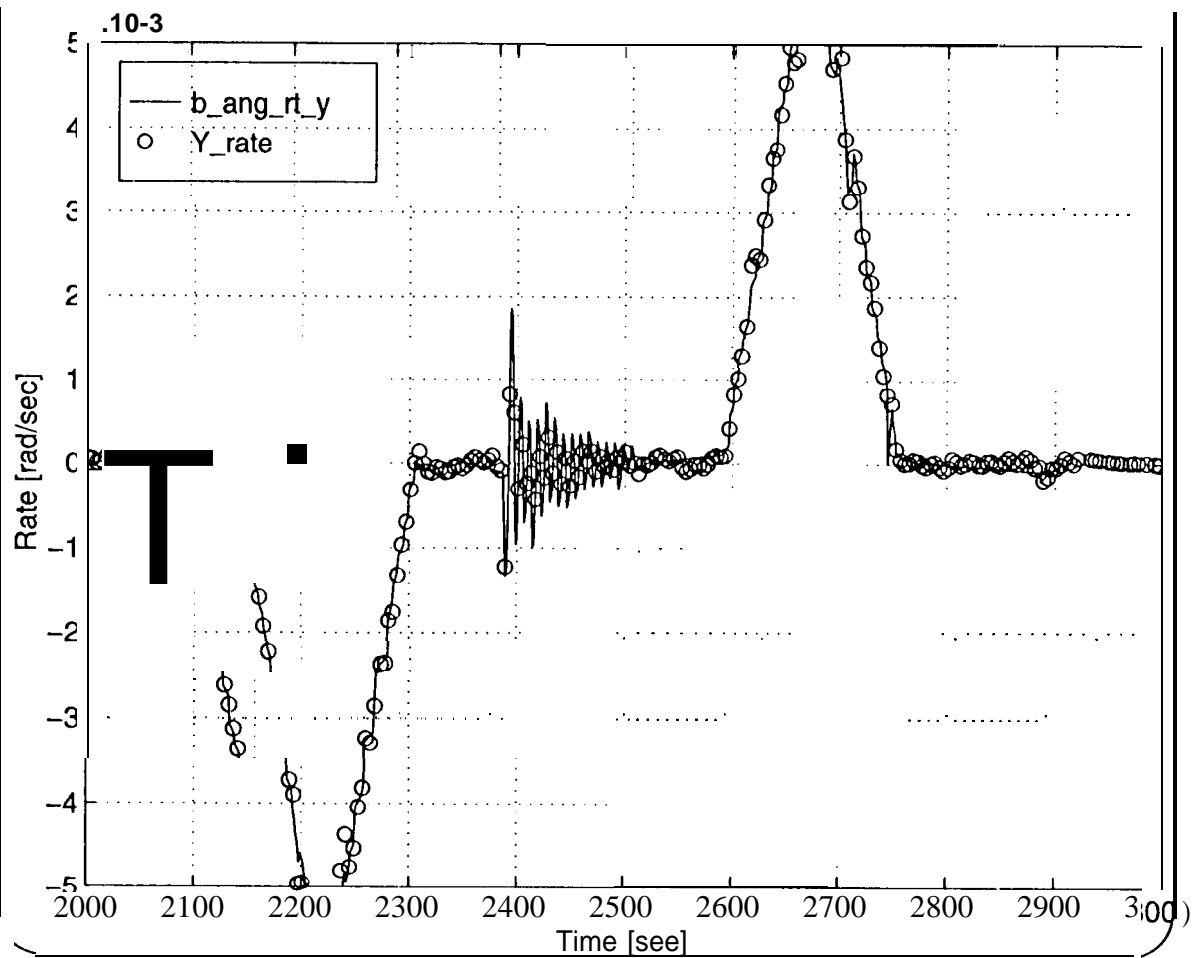


Figure 4-7 Simulated and Flight Software Angular Rates, Y Axis

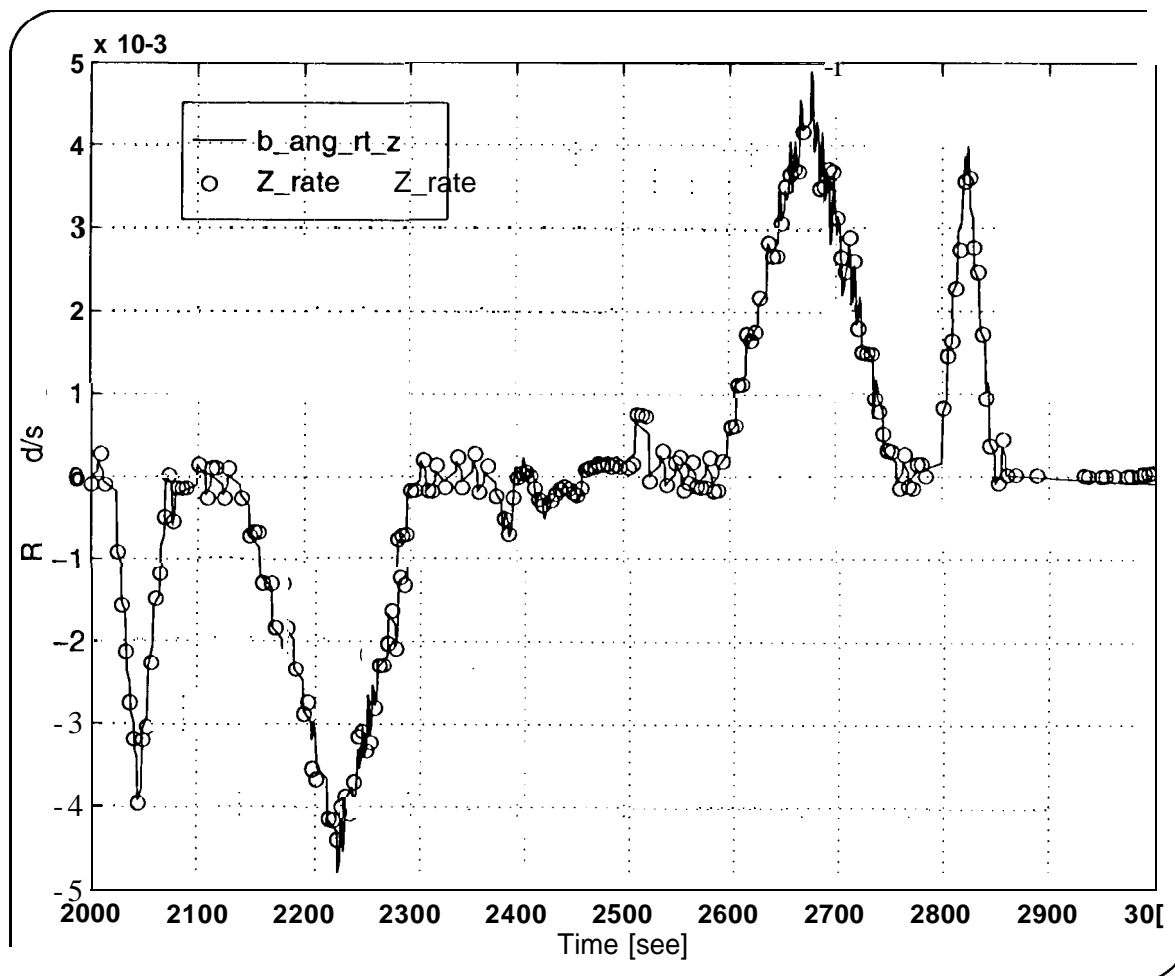


Figure 4-8 Simulated and Flight Software Angular Rates, Z Axis

or Z]_rate” is what flight software is reporting the angular rate to be after converting data from the IRU simulator. Both sets of rates track extremely well and we conclude that the IRU simulator performs well in the closed loop environment.

4.3 Evaluation

The Inertial Reference Unit simulator has performed very well in all three laboratories and has proven a valuable tool when IRU hardware was unavailable. The integration and test of the simulator revealed that the simulator had several shortcomings, but once these were corrected the simulator had a high degree of fidelity when compared to the actual hardware and closed loop performance during flight sequences have been excellent, The IRU assembly simulator represents the actual hardware well and, even though fault injection testing was limited, still performed adequately in ITL and CATS.

Chapter 5

Reaction Wheel Assembly

5.1 Description

The Cassini spacecraft has two sources of attitude control. The first source is the Propulsion Module Subsystem consisting of the main engines and 16 reaction control thrusters. The second form of control is the reaction wheel assembly. There are four reaction wheels on the spacecraft, three of which are the primary reaction wheels and the fourth which is a backup reaction wheel. The purpose of the reaction wheels is to store angular momentum of the spacecraft as well as to provide attitude control.

The reaction wheels receive commands from the flight software over the AACCS databus. There are eight commands that are accepted by the reaction wheels. These are summarized in table 5.1 below. [6]

Table 5.1: Commands and responses for the Reaction Wheel Assembly

Command	Response
Read Delta Angle	Return the accumulated angle count, (including over (under) flow indicator) and reset counter to zero.
Read Torque	Return the current command torque setting for the RWA
Read RWA Current	Return the current value of total RWA electrical current.
Read Motor Current	Return the current value of RWA motor electrical current
Read Status	Return the current operational status data of the RWA
Set Torque	Hold the reaction torque output at the value specified in the command
Reset	Set delta angle pulse counter to zero before resumption of counting, and set torque command to zero. This response shall be automatically executed at the time power to the RWA assembly is commanded on.

The reaction wheels utilize a brushless DC motor to spin the wheels and a hall effect tachometer to sense the motion of the wheel. Twenty four magnets are attached to the reaction wheel and hall devices sense the motion of these magnets past a sensor. This sensor then is the tachometer which increments by one each 1/24th of a revolution of the reaction wheel.

5.2 Cassini Laboratory Configuration

5.2.1 RWA Assembly Simulator

Description

As in the case of the IRU, the RWA assembly simulator consists of a remote terminal input output unit for the RWA, software for the simulation, and an interface card that permits communication between the two. The reaction wheel assembly simulation software is a C program that simulates the dynamics of the reaction wheel for the purpose of calculating outputs to communicate with the AFC via the RTIOU. The inputs to the program are torque command from the AFC and power on/off commands. The program's outputs are tachometer counts, wheel power, and a torque command wrap around. The program data flow consists of reading the power and torque commands, propagating a three dimensional state vector consisting of the wheel position, rate and a time dependent frictional term, and then computing the tachometer and power outputs for the AFC.

When the loop starts, the model reads a RAM register to determine if the AFC has commanded the wheel to power on. If the wheel is off, the power state is set to zero and the state continues to propagate. In that case, the model would simulate frictional spin down of the reaction wheel. If the wheel power state is set to one, the model performs two more reads of the RAM registers to read the torque enable command and the 2's complement torque command.

The second step of the loop is to propagate the state of the system. This is performed by computing the derivative of the state and then performing numerical integration to determine the actual state. To determine the derivative of the state, the program first computes the total torque that will be

applied to the wheel. This torque computation is shown in figure 5.1 and consists of four elements.

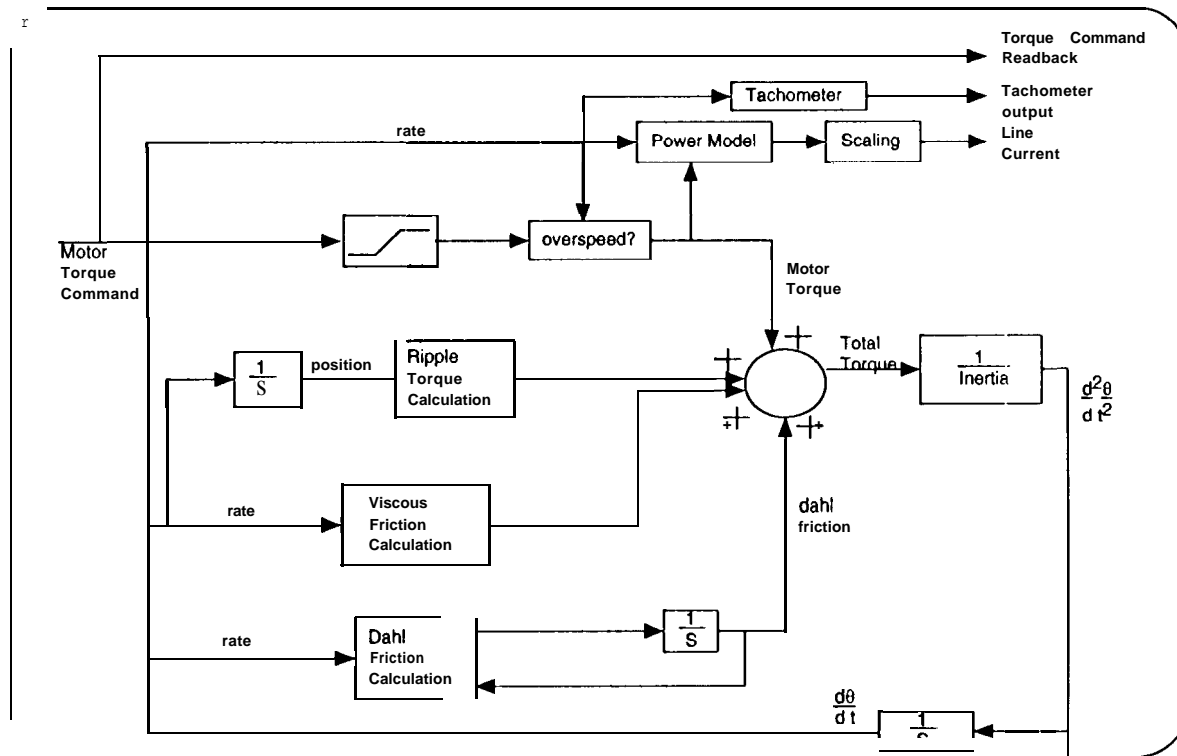


Figure 5-1 Reaction Wheel Assembly Simulator Torque Computation

First, there is the commanded torque. This is converted from two's complement to an equivalent value in Newton Meter-seconds and compared against a maximum motor torque. If the commanded exceeds the maximum, the motor torque is set to the maximum, There is **also** an overspeed flag that is set if the wheel is spinning too fast, If it is spinning too fast, the motor torque is set to zero. The second element of the torque command is a term to account for commutation ripple. This torque is due to the brushless DC motor and is sinusoidal in nature due to the switching of the DC current windings.

The third component of the torque is the viscous friction which opposes wheel velocity and is determined by multiplying the wheel rate by a constant. Finally, there is bearing friction to consider. This torque is called **Dahl** friction based on the bearing model developed by P.R. Dahl. [1] This model computes the time derivative of the friction and is integrated to determine the torque to apply. These four components are summed to determine the torque that will be applied to the wheel.

Once the torque is known, the state derivative is calculated. This is accomplished by setting the derivative of the position to the rate and the derivative of the rate to the torque divided by the wheel inertia. The derivative of the Dahl friction term is calculated via Dahl's model. These values are then used in a 4th order Runge Kutta numerical integration algorithm to determine the state of the system. The time step used in this routine is 0.0625 seconds.

Finally, the output is computed. This is performed by first calculating the power consumed by the wheel based on the vendor's power model and converting the power into a current. Next, the tachometer data is computed. This simulation runs every 62.5 ms, but the tachometer data is read by the flight software every 125 ms. Therefore, the tachometer output should reflect what the real tachometer would say after 125 ms. This is accomplished by multiplying the current rate of the wheel by 125 ms. This gives an estimate of the position of the wheel after 125 ms. Then, this is multiplied by a scale factor representing the **quantization** of the tachometer. This is then the output of the tachometer. Since the output is an integer, the fractional value computed by this calculation is saved and added to the next read. In this manner, no tachometer counts are lost. Finally, the current, tachometer counts, and the torque command are sent to the RAM registers for transmission through the RTIOU back to the AFC.

Validation Testing and Results

The reaction wheel assembly simulator was unit tested by performing the reaction wheel simulation integration procedure in the ITL, CATS, and ALTO. This procedure contains power off and power on tests to verify electrical interfaces between the AFC and the RWA simulators. The power off section is performed with break out boxes in the loop to protect the hardware in the event of an incorrect connection. The power on tests verify that the flight software can command the wheels and that the reaction wheel simulation responds as expected. These tests were performed in the ITL and in CATS and no significant problems were found that would inhibit testing using the simulators.

A second set of tests was also performed. This set duplicated tests that were performed on the flight equipment during stand alone testing. These tests were performed in CATS to allow for comparison of simulator response and that of the actual hardware. The results of this test are shown

in figures 5.2 and 5.3. Figure 5.4 shows the error between the two rate plots.

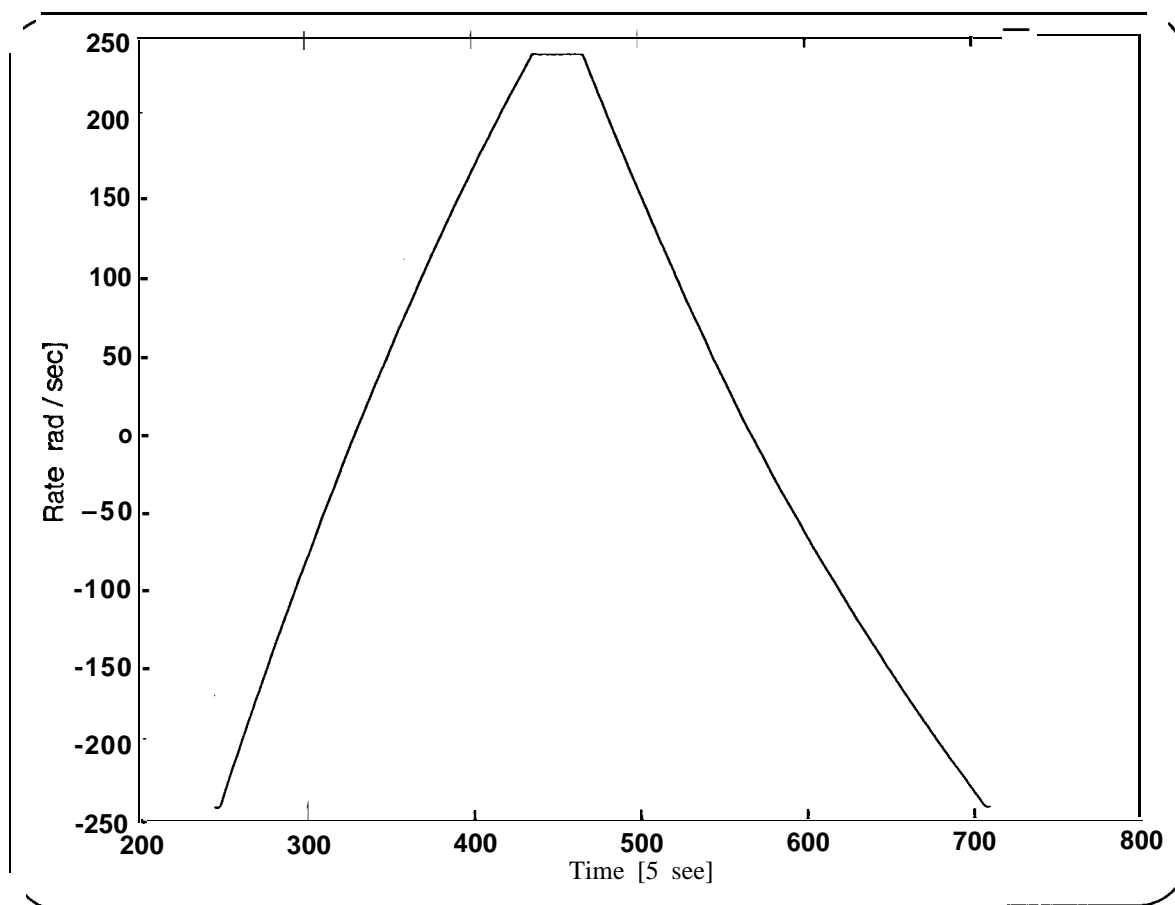


Figure 5-2 Reaction Wheel rates during comparison test

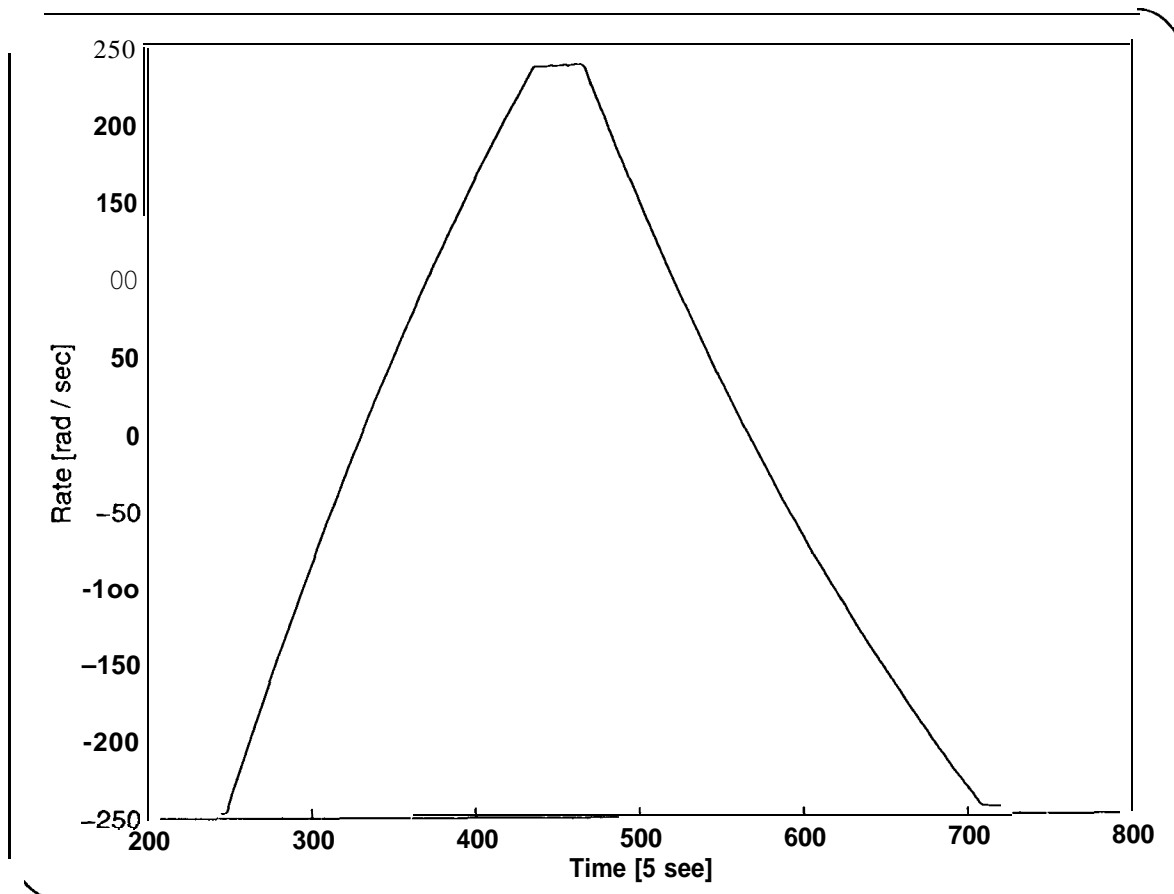


Figure 5-3 Reaction Wheel simulator rates during comparison test

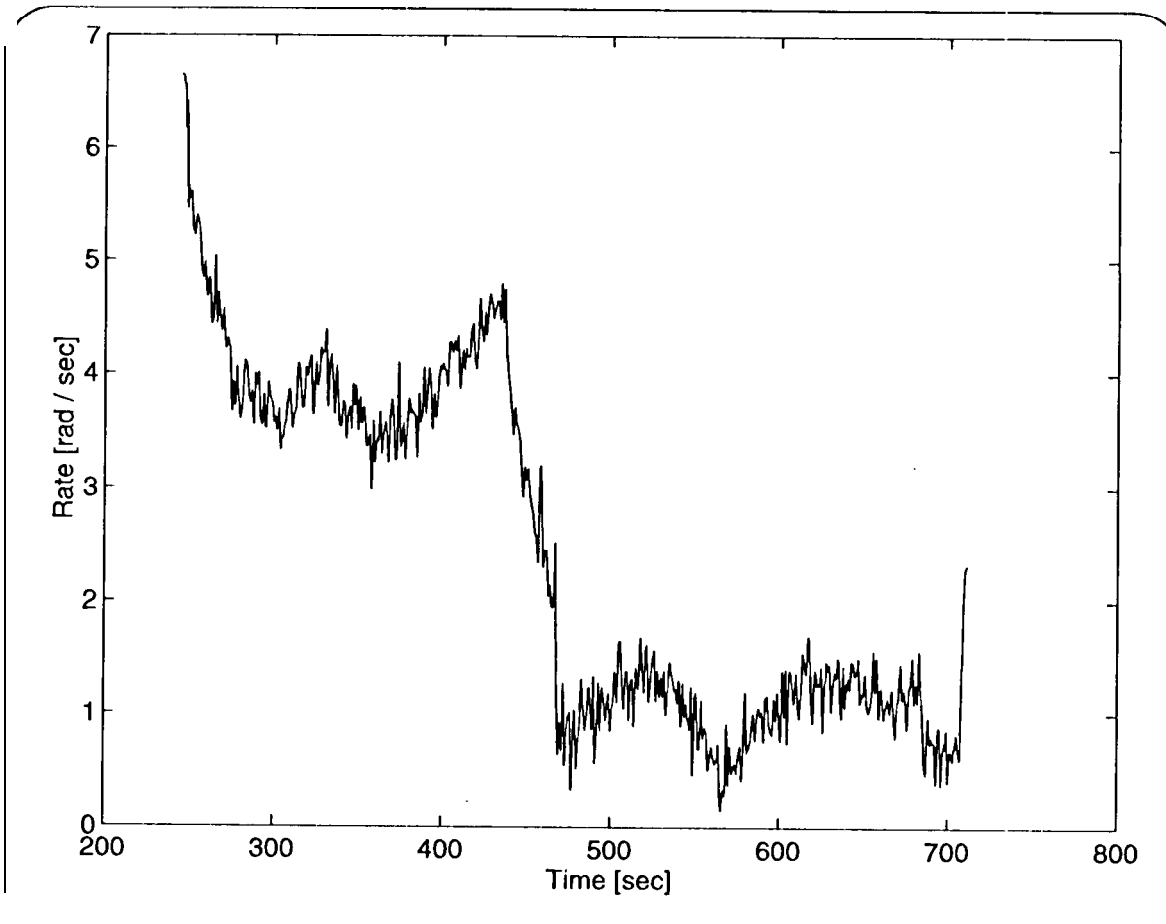


Figure 5-4 Error between reaction wheel simulator and hardware

As is shown in the plots, particularly in the error plot, the simulator was able to track the hardware quite well. The initial error is essentially a result of not being able to exactly reproduce the earlier test. The hardware was tested in a stand alone environment, while the simulator was tested with flight software active. As a result, the simulator test was subject to flight software constraints on allowable wheel torques and rates. However, during wheel rate changes on the order of 500 radians per second, the error was less than 10 radians per second. In addition, this error did not change appreciably when the wheels were accelerating.

There are a number of important differences between the simulation and the real reaction wheels. The first difference is the multiplexer that exists on the real wheel. This allows the flight software to receive different measurements of reaction wheel current and voltage. However, flight software is not designed to use any information other than the line current for the reaction wheels. Thus, the

simulator only computes line current.

A second difference points to an important issue that was seen earlier with the IRU simulator. Neither of these simulators have any knowledge as to when the flight software is going to read the RTIOU output. This means that information must be kept current at all times at the RTIOU output. A consequence of this is seen in the way the output of the RWA was computed. The RWA routine runs at 16 Hz, but the flight software reads the RTIOU of the RWA at 8 Hz. Thus, it would be desirable to run the output routine at 8 Hz as well. The problem is that if this is attempted, the simulator and the flight software diverge from each other and the result is incorrect output. “Old” information is kept at the RTIOU registers for too long and incorrect information is relayed to flight software. This is why the output routine runs at 16 Hz and integrates the tachometer output as if it was running at 8 Hz. This way, the simulator and the flight software will not diverge enough to cause problems. In addition, the reaction wheel simulator will use the signal from the assembly simulator card indicating a flight software read to prevent data corruption.

A third difference lies in the fact that the static ram that allows communication between the software and the RTIOU uses the same registers for reading and writing. That is, the memory location for reading information from a register is the same that is used to write information to that register. This is a problem with register 5 of the RWA. This register is simultaneously the lower byte of the tachometer data from the RWA simulator and the load mux command to the RWA. This means that there is a chance, if the timing is unfortunate enough, for the RTIOU to read what it believes is the lower byte of tachometer output, but is actually the old load mux control command from that last cycle. This is a rare occurrence due to the faster processing time of the RWA simulator, but if the processing takes excessively long or if flight software is quicker than usual, bad data could reach the AFC. With the real RWA, read and write registers are separate, but this is not the case with the simulator and thus this danger exists.

One of the most difficult features of the reaction wheels to simulate was the response of the reaction wheel to a reset of its Remote Terminal on the AACS databus. A reset of the remote terminal input/output unit (RTIOU) can occur one of three ways: the RTIOU can be commanded to reset, it resets as a result of a power on, or the RTIOU can reset due to a timeout. A timeout occurs when the RTIOU does not receive a command for 250 ms. An RTIOU reset results in the reaction wheel setting its torque command to zero until further instructions are received from flight software. This prevents the reaction wheel from acting on an incorrect or obsolete torque command and spinning

out of control. Furthermore, the reaction wheel hardware manager inside flight software expects to read a zero torque value back from the reaction wheel and will not command the wheels until this zero is received.

The problem with simulating this reset response is threefold. First, the static RAM card that allows the reaction wheel simulation software and the **RTIOU** to communicate does not include a channel to relay the **RTIOU** reset information to the reaction wheel assembly simulator. Therefore the software had no direct knowledge of the **RTIOU** reset. Secondly, the static RAM uses the same memory locations as read and write registers. This means that if an **RTIOU** reset was detected falsely and the software wrote a zero to the torque memory location, good torque commands would be overwritten. The final difficulty is that the flight software and the reaction wheel simulator have no knowledge of each others timing. A reset could occur anytime during the simulators processing cycle and the software would have to somehow correctly write a torque command of zero when a reset occurs.

The first attempt to solve this problem is depicted in figure 5.5. The software nominally runs twice

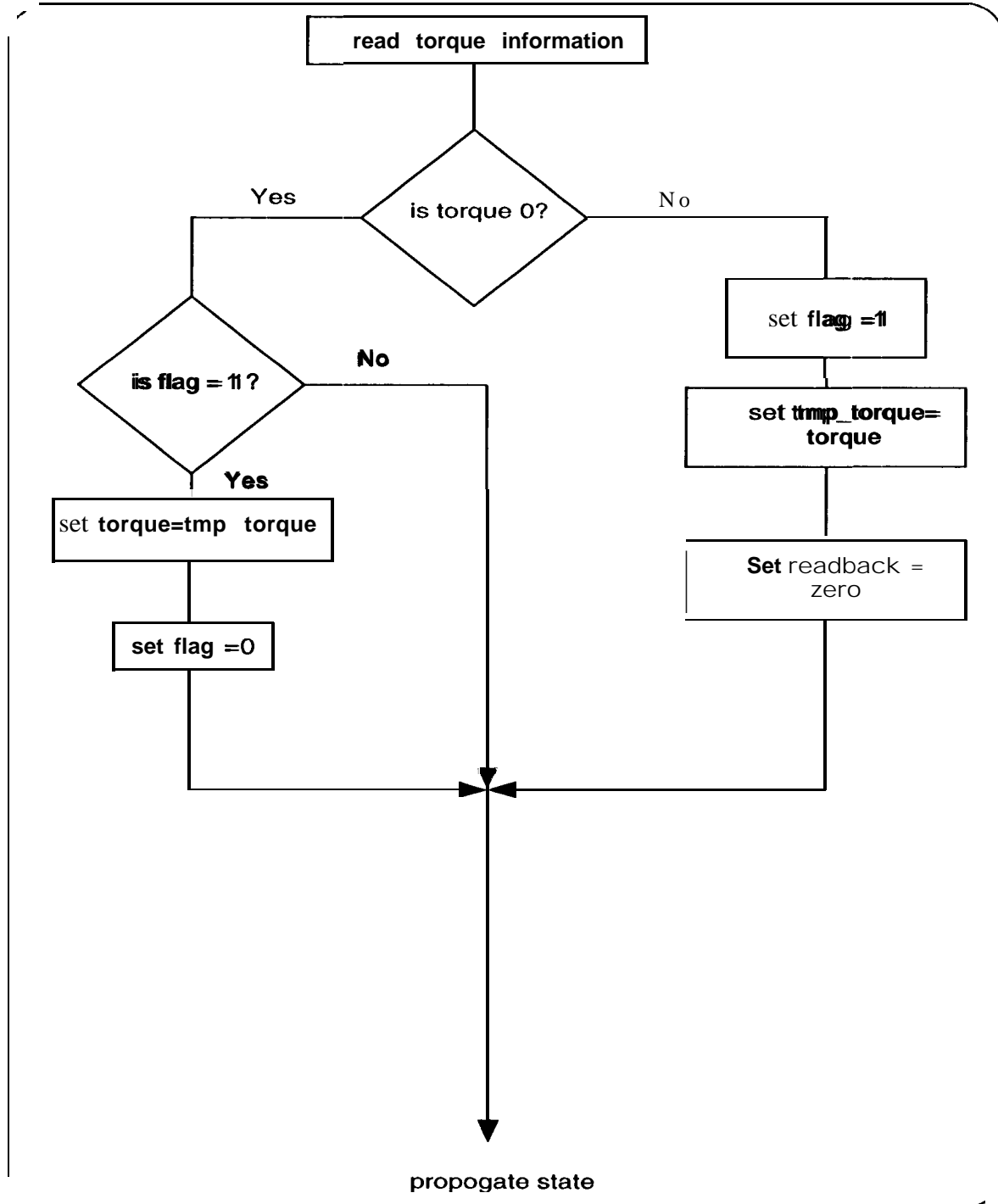


Figure 5-5 First attempt in solving remote terminal reset anomaly

as fast as the flight software, so the simulator should expect a new torque command every other cycle. The first action is to read a new torque command and overwrite the RAM memory location with a zero. Then the simulation continues using the read in torque command. It also copies the command to a temporary buffer. The next cycle, the software expects a zero (which it wrote) since no new update has occurred. If this is true, the software acts on the previous torque command that was buffered and propagates the state again. Finally, the register is read a third time. If the zero is still present, the software assumes that a reset has occurred since it did not receive a new update and thus acts on the zero until a new update is received, when the cycle begins again.

This method did not work well. The software overrode the good torque commands with zeros incorrectly and the simulator failed. This was caused by the fact that flight software timing is not exact and synchronizing the simulator and flight software was too difficult in a real time environment. This can be seen by examine the following databus transactions

96-264/1 8:30:52.153 bm_d_rwx2 = 000eae0407074001004006 65 c096

96-264/1 8:30:52.235bm_s_rwx2 = 00 100706ae09e00000ff000d91 65 c072

96-264/1 8:30:52.278bm_d_rwx2 = 000eae0407074001004006 65 c096

96-264/1 8:30:52.360bm_s_rwx2 = 00100706ae09e00000ff000d91 65 c072

96-264/1 8:30:52.403 bm_d_rwx2 = 000eae0407074001004006 66 c094

96-264/1 8:30:52.548bm_s_rwx2 = 00 100706ae09e00000ff000e89 00 c093

96-264/1 8:30:52.590bm_d_rwx2 = 000eae0407074001004006 00 c061

96-264/1 8:30:52.673bm_s_rwx2 = 00100706ae09e00000ff000d89 00 c08f

96-264/1 8:30:52.715 bm_d_rwx2 = 000eae0407074001004006 65 c096

96-264/1 8:30:52.860bm_s_rwx2 = 00100706ae09e00000ff000e89 00 c093

96-264/1 8:30:52.903 **bm_d_rwx2** = 000eae0407074001004006 00 c061

96-264/1 8:30:52.985 **bm_s_rwx2** = 00100706ae09e00000ff000d89 00 c08f

96-264/1 8:30:53.028 bm_d_rwx2 = 000eae0407074001004006 65 c096

96-264/1 8:30:53.110 **bm_s_rwx2** = 00 100706 ae09e00000ff000e9 1 65 c076

96-264/1 8:30:53.153 bm_d_rwx2 = 000eae0407074001004006 66 c094

This data is from testing on GMT day 96-264 in CATS. Data denoted at **bm_s_rwx2** are source bus packets for RWA2 (from RWA2) while those denoted as **bm_d_rwx2** are destination bus packets for RWA2 (from the AFC). Appendix A has a complete RWA bus data decoder. the critical information is decoded and explained below.

The first source packet contains a OX66 (denoted by the spacing before and after) which is the torque command read back from the reaction wheel. (OX66 = 102 dn [dummy units]. This corresponds to a torque of 0.14 Nm) The next destination packet writes a 65 to register 6 (the torque register). This is acted upon and the RWA reports back a 65. This happens again with no incident. But observe what happens at 18:30:52.403. The flight software commands a torque of 66, but the RWA is delayed in responding until 18:30:52.548. Since the flight software commands a reading from the reaction wheels about 4 ms before the **bm_s_rwx2** data appears, this corresponds to a delay between flight software commanding a torque and reading the reaction wheel of over 140 ms. This delay results in the simulator reporting a zero as a read back, since the software believed an RTIOU reset had occurred. Flight software responds by requesting a zero and verifying it reads back a zero. This happens at 18:30:52.673 and thus flight software commands a torque of 0x65 to resume processing. But again a delay occurs and the torque returns to zero. The simulator/flight software combination break this pattern at 18:30:53.028 and nominal operation continues.

Bases on this information, it was deemed essential to support as many as three simulation iterations between flight software commands as well as to minimize the writing of zeros to the torque command. A new method was devised to met these additional requirements.

This new method is shown in figure 5.6. This method uses the torque enable flag, which is set to

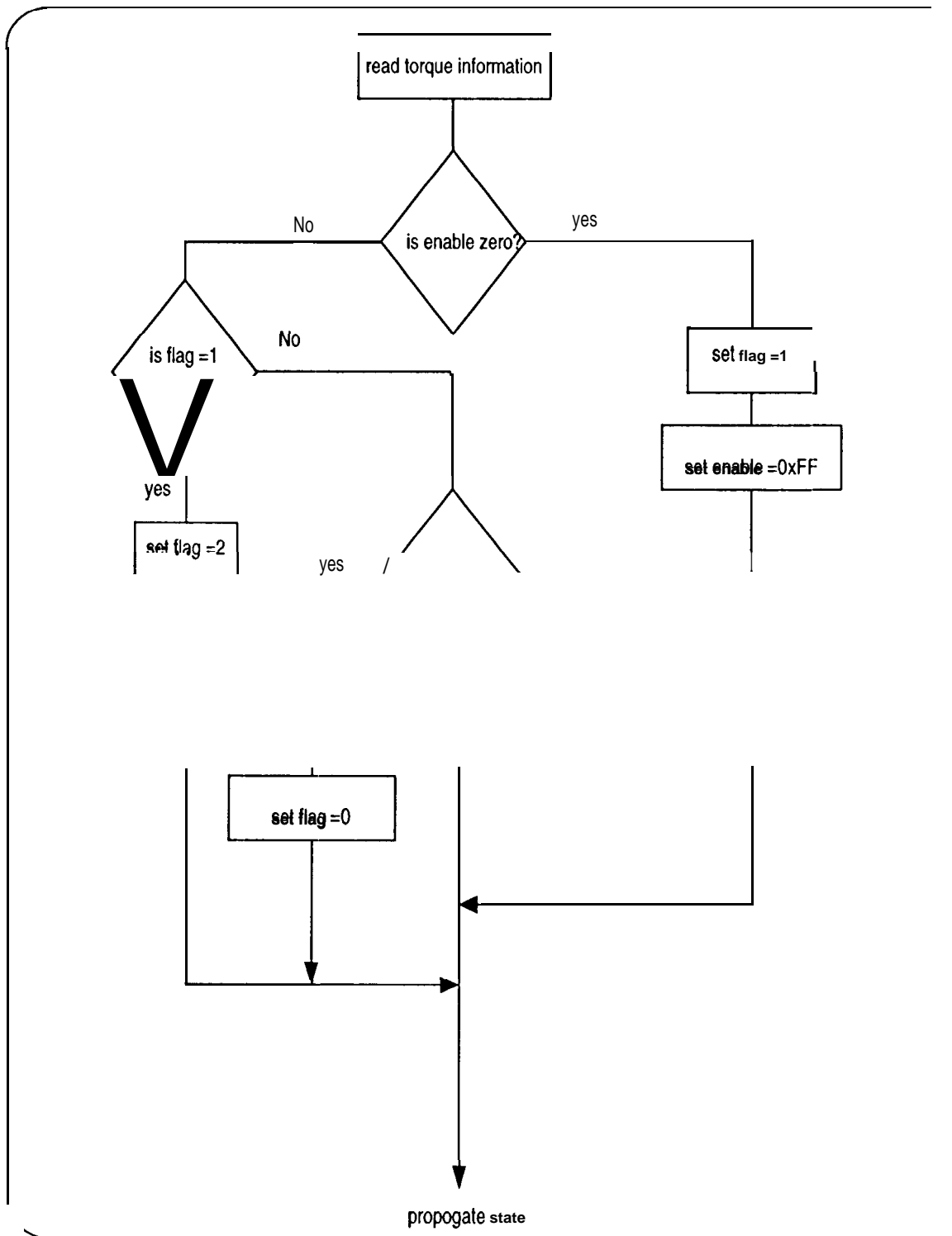


Figure 5-6 Second attempt to solve Remote Terminal Reset Anomaly

zero by the flight software each time a torque command is sent. The torque enable command is monitored at the beginning of each iteration. If the torque enable command indicates new data has been received, then the simulation accepts this data and resets the torque enable command. The simulation then acts on this new data until 3 cycles without an update are complete. Then the simulation software sets the torque command to zero and acts on it as well. Thus the torque is set to zero only if no updates are received for three cycles.

This method was much more successful and the results can be seen in figure 5.7. The reaction wheel

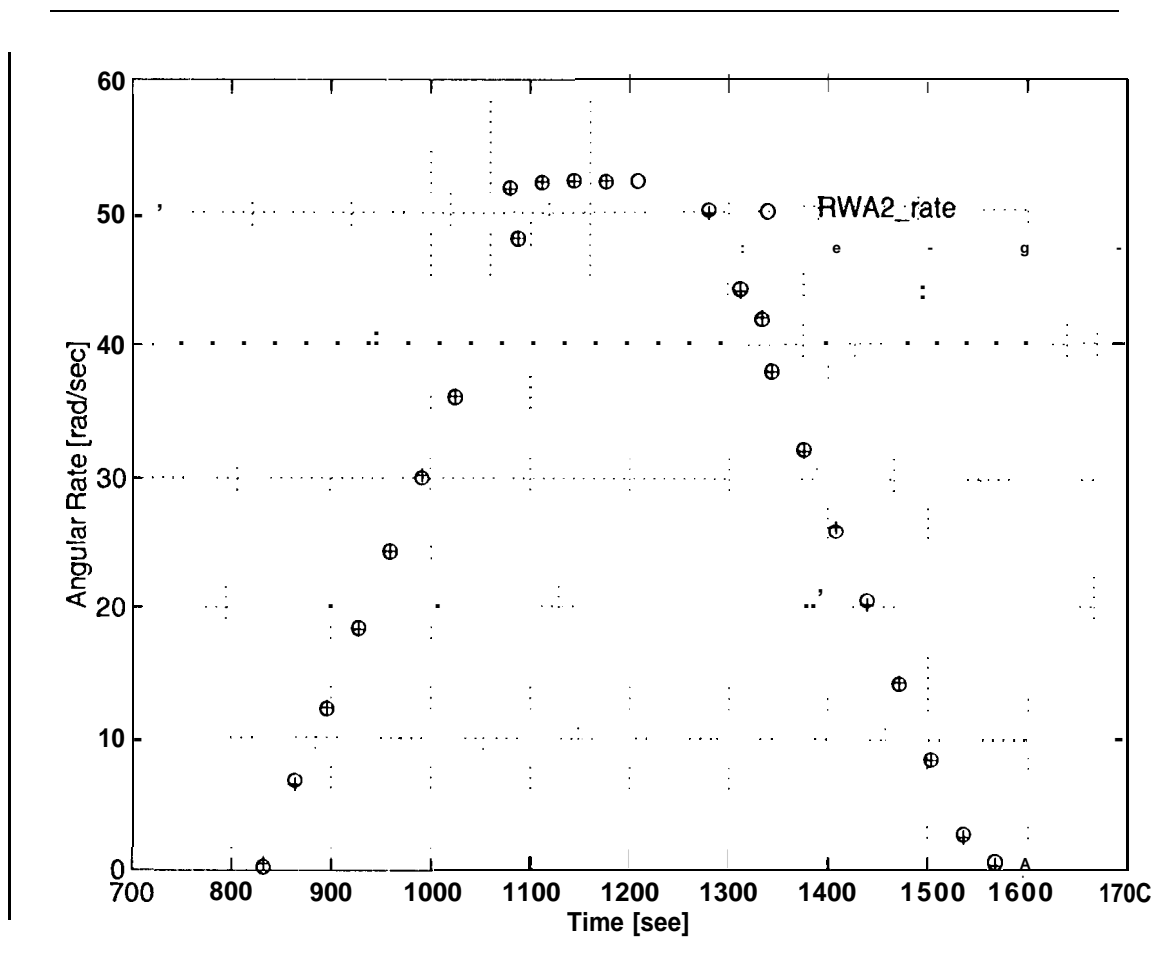


Figure 5-7 Successful retest of remote terminal reset anomaly

rates follow the idea rates computed by flight software very closely and the torque command remained constant even in the presence of an RTIOU reset.

This modeling revealed an important consideration in real time simulation. It is critical that the

simulated wheels have the same access to information that the hardware does. The reaction wheel simulator does not have a reset line, nor does it have separate input and output registers. This lack of information made the RTIOU reset response a much more difficult item to model. This is an area for improvement for Cassini's Reaction Wheel simulator. The presence of a torque enable command was fortunate and allowed the software to model the reset response, but the software response is different from the real hardware because the software and the hardware have different information available to them.

A final concern is the impact on fault injection. It has been decided that no fault injection would be conducted in the ITL or CATS with the RWA simulators. This is due to the same decision that impacted the fault injection of the IRU. Since no real command path exists to bias the tachometer of a real wheel, no attempt will be made to do the same with the simulator. In addition, the timing issues discussed above makes it impossible to guarantee that a particular flight software command will generate a particular response, so injecting faults such as an incorrect torque readback during a flight software cycle is not possible to simulate.

5.2.2 RWA Dynamics Model

Description

The reaction wheel dynamics model consists of a C program that is designed to simulate the reaction wheels in order to generate torques to apply to the spacecraft dynamics model. The model receives three pieces of information from the assembly simulator described in 5.2.1 above: the commanded torque which is read back from the assembly simulator, the tachometer reading from the assembly simulator and the time of the torque command read back. This information is used to drive the dynamics model as shown in figure 5.8. The first step is a call to DARTS to compute the angular rate of the modeled wheels. Once the rates are known, the model computes a rate error. First, the time since the last calculation is computed from the timing information. Second, a rate sample is calculated using the tachometer output and the elapsed time since the last calculation. This rate sample is put through a low pass filter that combines the rate sample with a previous rate estimate to obtain a new rate estimate. The purpose of this step is to limit the amount the rate estimate can jump in any one iteration. This rate estimate is then used with the rates of the DARTS wheels to obtain the rate error.

Once the rate error is known, the model computes the torque to be applied to the simulated wheels

inside DARTS. First, a correction torque is computed. This correction torque is a function of an estimate of the drag torque and the rate error. The rate error is also used to compute the next value of the drag torque estimate. Finally, the torque applied is computed by subtracting the correction torque from the commanded torque.

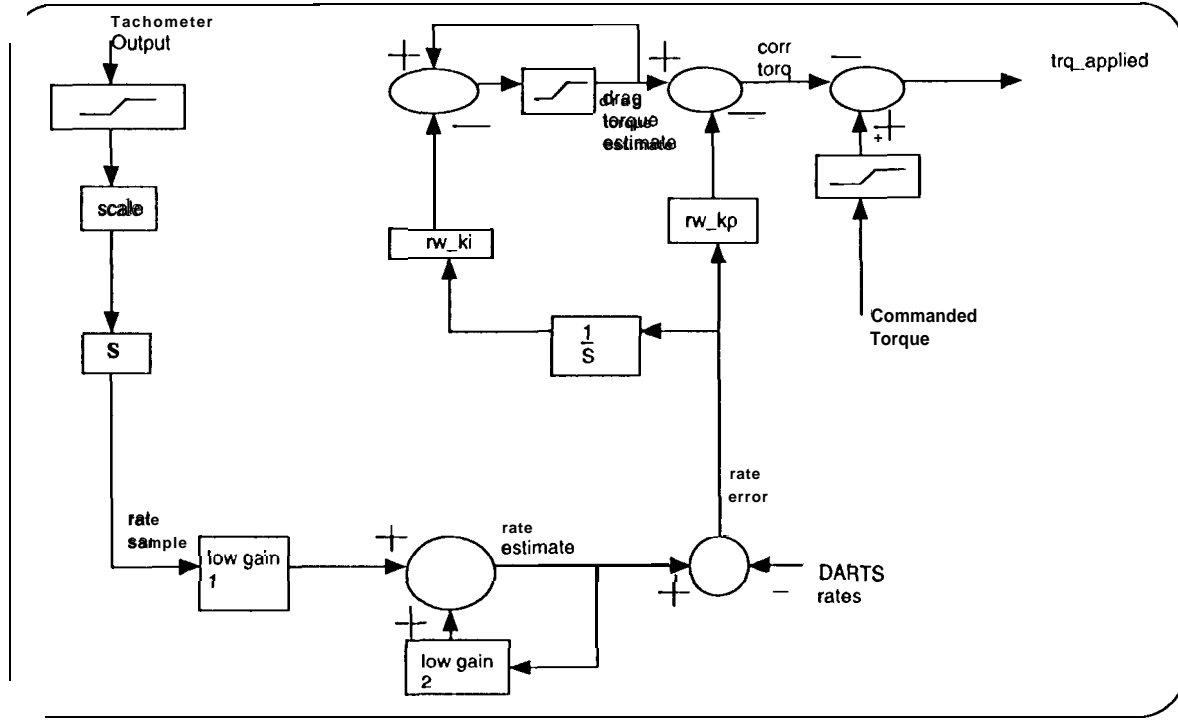


Figure 5-8 Reaction Wheel Dynamics Model Controller Block Diagram

Validation Testing and Results

To validate the model, conservation of angular momentum was invoked to develop predicts for the simulated spacecraft rates as follows:

$$H = I\omega \quad (5.1)$$

$$I_{XX,S/C} \omega_{X,S/C} + I_{re} \omega_{re} l_X \quad (5.2)$$

$$\omega_{X,S/C} = \frac{I_{rw} \omega_{rw} l_X}{I_{XX,S/C}} \quad (5.3)$$

Where

$I_{XX,S/C}$ = Principle Moment of Inertia, X axis, Spacecraft

$\omega_{X,S/C}$ = Angular Velocity about X axis, Spacecraft

I_{RW} = Moment of Inertia, Reaction Wheel

ω_{RW} = Angular Velocity, Reaction Wheel

l_x = Direction Cosine transform from reaction wheel to Spacecraft

Therefore, the effect of a reaction wheel's velocity on the spacecraft could be predicted, knowing the moments of inertia of the spacecraft and reaction wheel, as well as the transform from reaction wheel to spacecraft. The results of the testing was that after several coding errors were discovered and fixed, the model did match analytical predicts to within $1 \text{ e-}4$ radians/second. Model Validation uncovered one particular feature of the real time simulation that almost prevented the dynamical wheels from functioning before it was fixed. The problem was with the corruption of data coming to the simulator from the blackboard. The simulator assumes that the data it receives is valid and relies on this information to track the reaction wheels on the spacecraft side of the simulation (real or simulator). This means, for example, if the **timetags** used to **determine** the new speed of the spacecraft wheels are corrupted and the change in time is falsely computed to be extremely small, the model will compute an unusually large rate estimate and attempt to torque the dynamics wheel to match this incorrect rate estimate. This resulted in several problems that had to be cor-

rected. For example, figures 5.9 and 5.10 shows data from GMT day 96-233 and 96-235 where

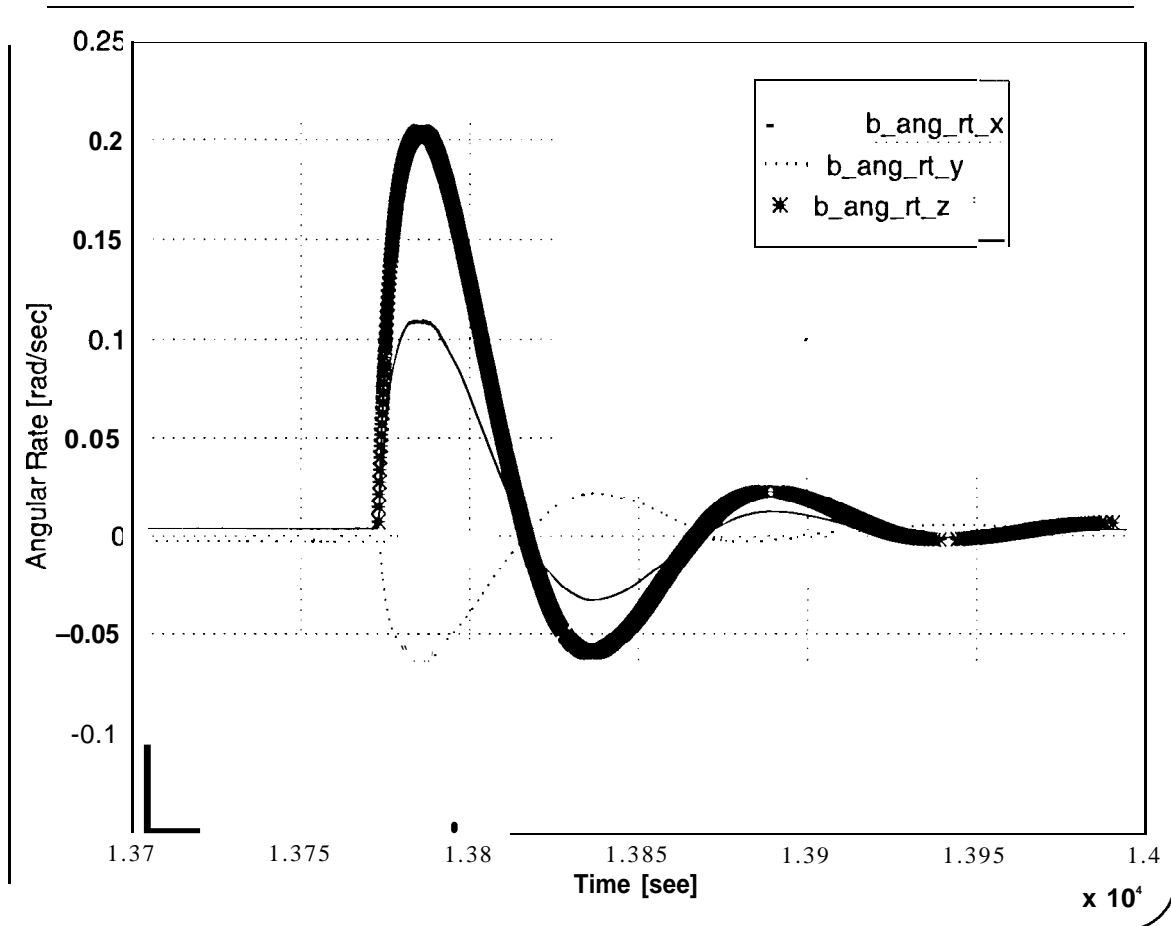


Figure 5-9 Reaction Wheel dynamics simulator anomaly- 96-233

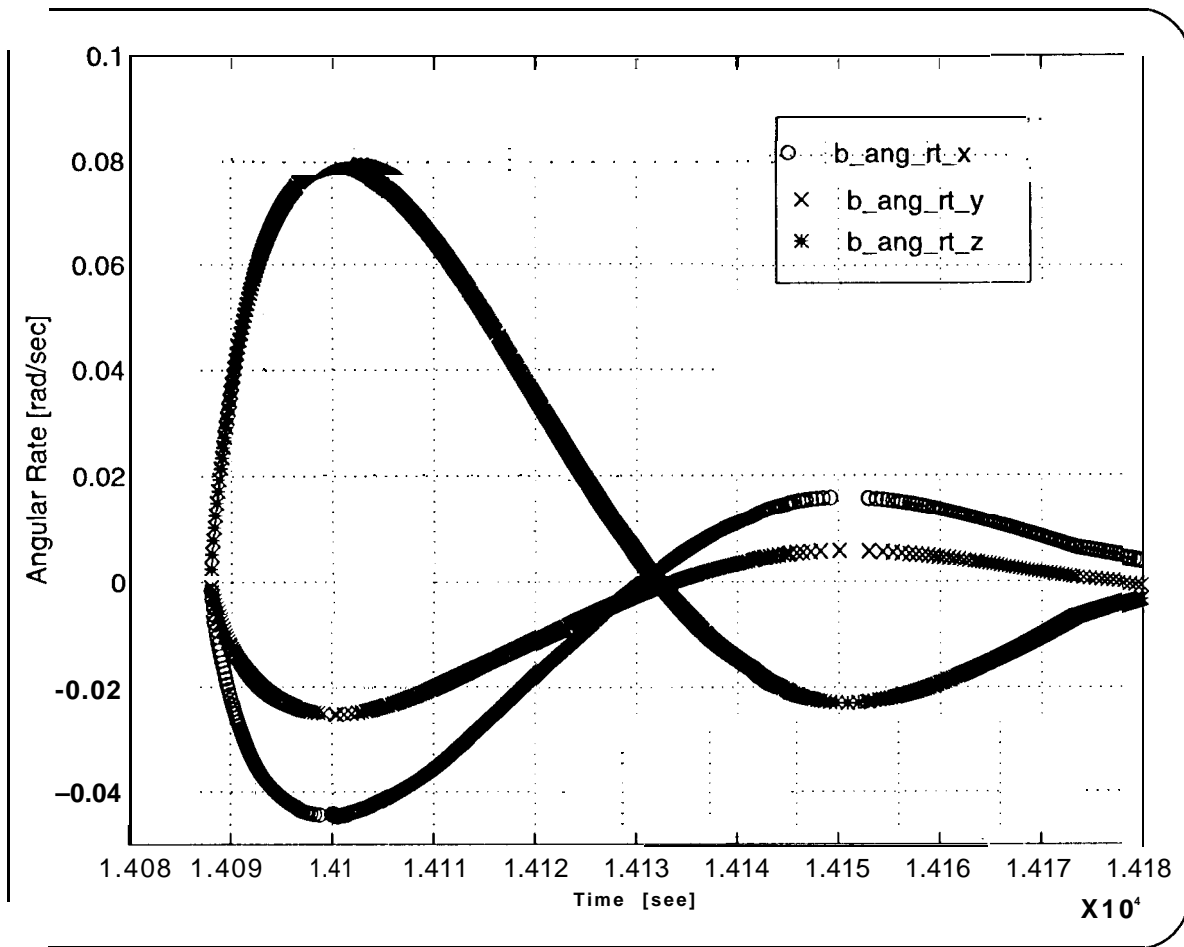


Figure 5-10 Reaction Wheel dynamics simulator anomaly- 96-235

the reaction wheels spun out of control and later recovered. Examination of the model software revealed that this second order behavior would be possible if the software received a small change in time estimate (used in the computation of the rate sample and the drag torque estimate). This would result in a torque sent to the dynamics wheels that would be unrealistically large based on the unrealistic speed and drag torque computed, and the rates would jump as shown. When the next update was reasonable, however, the rates would decrease and the wheels would gradually be brought under control. The response is second order due to the proportional plus integral controller used in the dynamics model. To “correct this, a limiter was added to the drag torque estimate (shown in figure 5.8). Filters were also added to the incoming tachometer and torque data, as well as software to limit the change in time estimate to within 25 ms of the expected value. Initially, the necessity of the limiter on the change in time estimate was not discovered and when the time

is was not limited (and only the drag torque, torque and tachometer filters were activated), the error became a first order response, shown in figure 5.11. This is because the drag torque filter limited

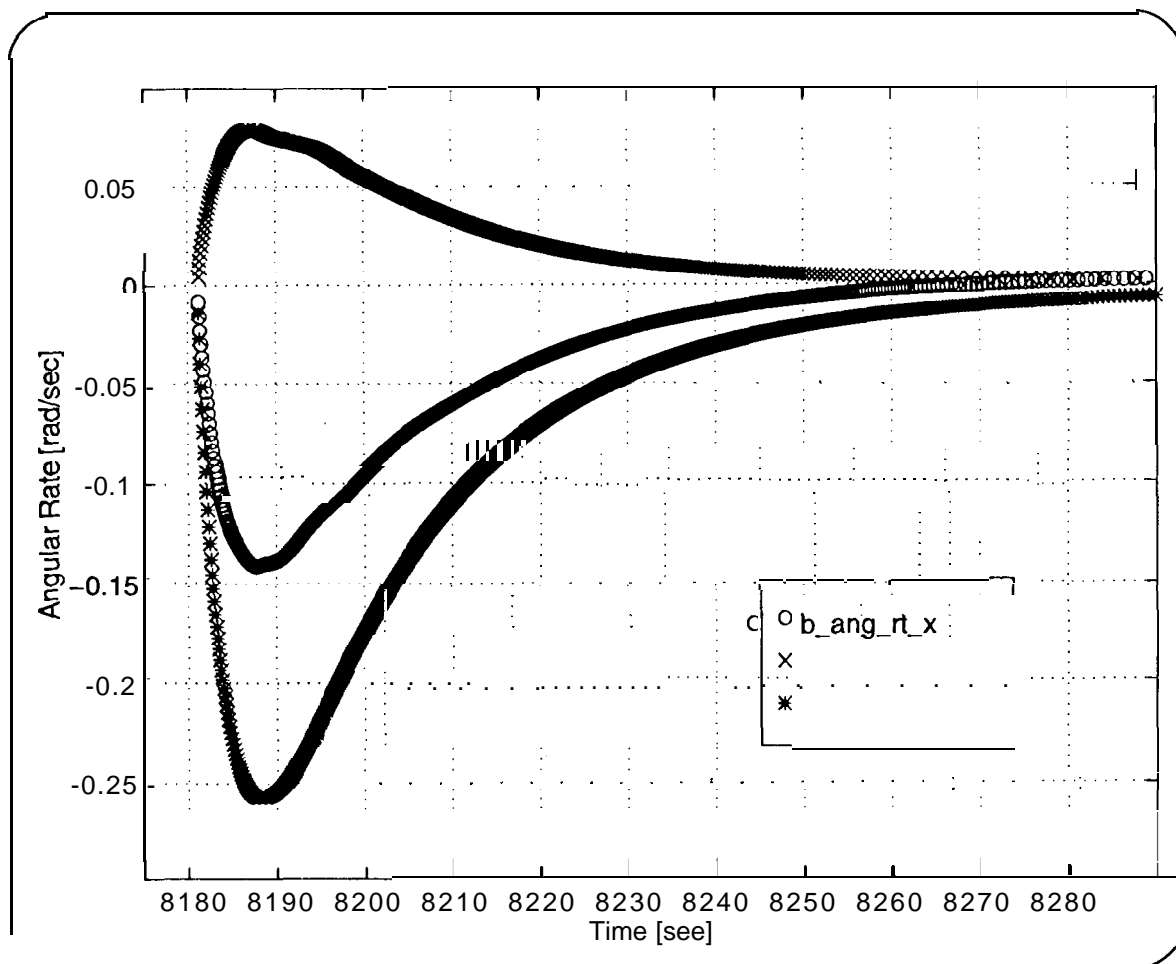


Figure 5-11 Reaction Wheel dynamics model first order anomaly

the integral controller, but not the proportional controller could still be in error if a large, incorrect rate sample was computed. Once the change in time computation was limited, the model did behave as expected with no anomalous error responses.

5.2.3 Closed Loop Simulation

A closed loop flow diagram is shown in figure 5.12. This configuration was used to test the AACS

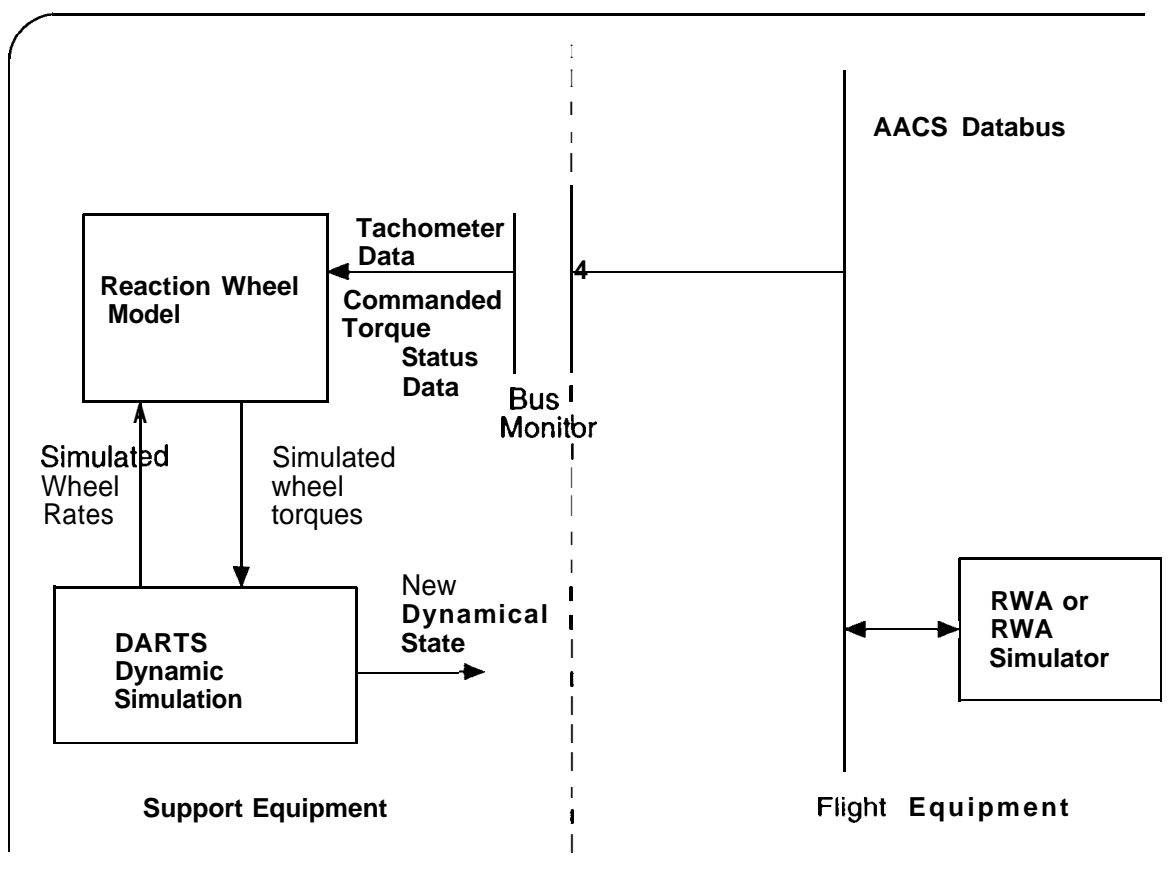


Figure 5-12 Reaction Wheel Simulation closed loop diagram

during the operational modes (OPM) sequence testing. The OPM sequences test the reaction wheels during a series of precision pointing maneuvers simulating science data gathering operations when Cassini performs its orbital tour. The desired profile of the spacecraft angular rate is

shown in Figure 5.13. The data was generated during flight software testing on the Flight Software

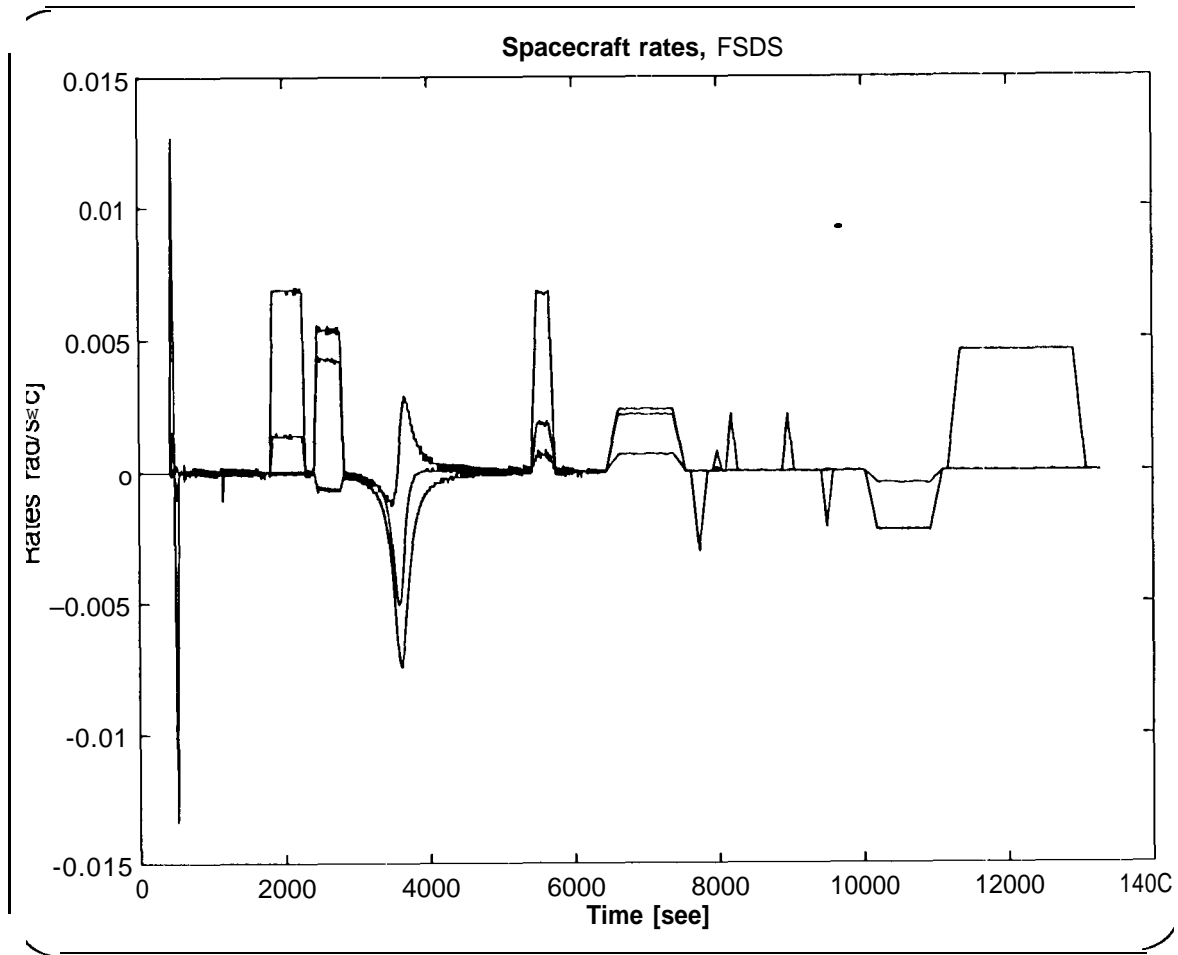


Figure 5-13 RWA OPM Testing- Flight Software Development Station

Development Station (FSDS). The next figure, 5.14, shows the results from the testing in CATS

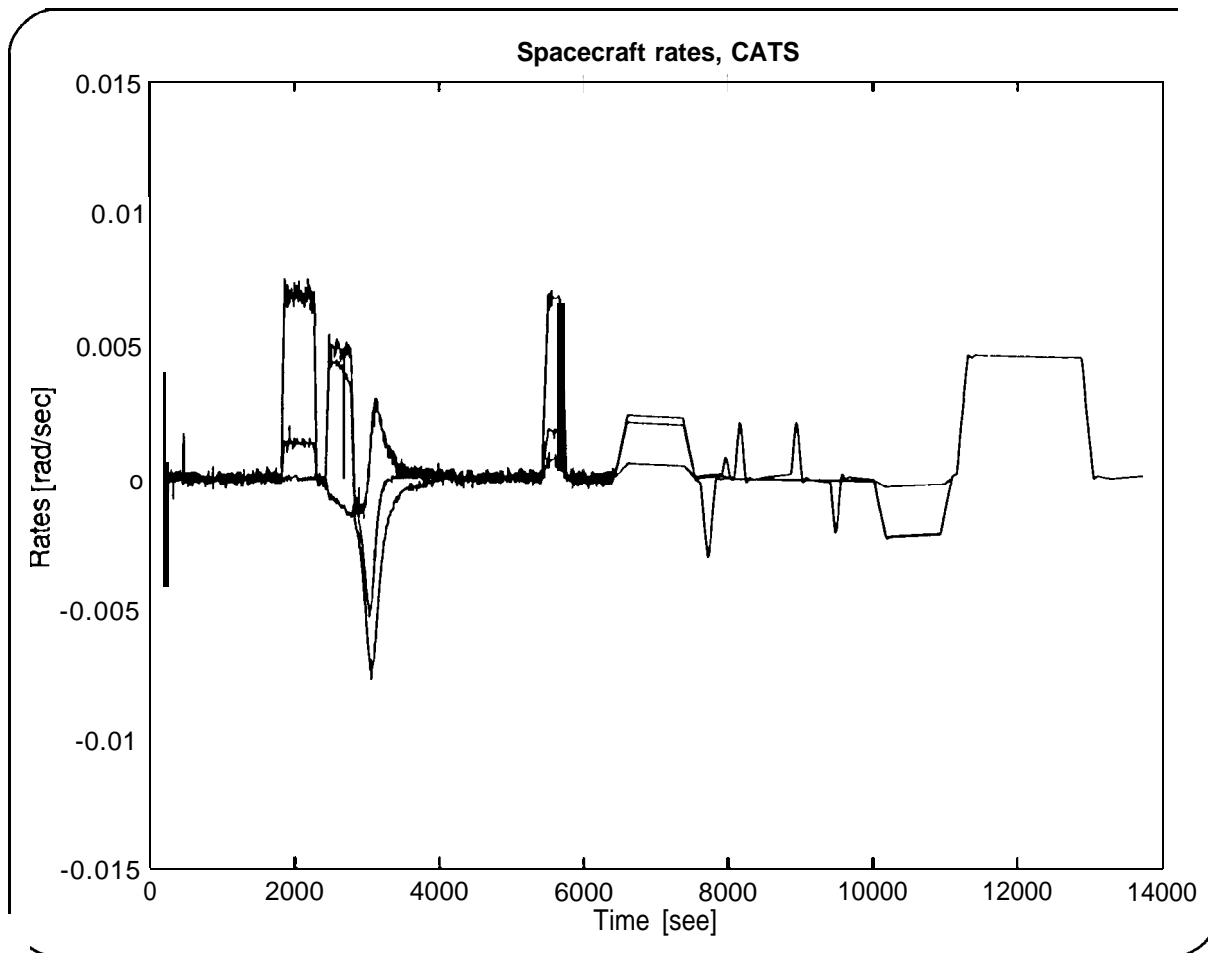


Figure 5-14 RWA OPM Testing- CATS

on GMT day 96-237. The spacecraft is under reaction wheel control for the second part of the sequence. This section can be identified by the reduction in noise of the rate plots. The CATS tests matches very closely with the FSDS run and the closed loop performance of the RWA simulator and the dynamics model was verified.

An important lesson that was learned during the RWA closed loop testing is the value of simulators when software is being tested. As the complexity of software grows, the chance that something will operate incorrect] y grows as well. This is evident from several flight software tests when the software reaction wheel manager was acting incorrectly and was sending torque commands to the reaction wheels periodically. If these commands were sent to the real hardware, the results could

have been very unfortunate and the hardware may have been damaged. Thus, the simulators played a critical role in closed loop software testing as well.

5.3 Evaluation

The reaction wheel simulator is the most complicated software simulator due to its internal dynamics and the importance of timing associated with it. Both functionally and in performance, the RWA simulator closely matched the **real** hardware. The laboratories relied heavily on the simulators during testing and they performed their functions well. Validation activities for the reaction wheels revealed the problem of data corruption within the simulation. This problem was surmounted by implementing filters on incoming reaction wheel data. The fact that the flight and **support** equipment software do not talk to one another resulted in a difficult implementation of the reaction wheel **RTIOU** reset response as well. However, even with these problems, the RWA simulator permitted effective testing of the AACS.

Chapter 6

Conclusion

This thesis has investigated the use of simulators during the testing of Cassini's AACS. The simulators have all met their requirements and testing in the three laboratories was improved through the use of these simulators. There are several lessons that have been learned during the testing period.

The first lesson is the importance of clear requirements and objectives in simulation. For example, the fact that the EGA simulators were never meant to simulate a leaded EGA led to the activation of fault protection during ATLO testing. It was the misunderstanding of this fact that led to the fault protection event. An example of clear requirement understanding is the IRU SHARC simulator. It was clear from the beginning that "the support equipment software would not simulated the actual BIT or software download. Since this was specified, testing of these functions was handled elsewhere and this clear expectation led to effective testing.

A second lesson is that there is a tradeoff when deciding on additional command paths in simulators. The Cassini project decided not to add any additional command paths. The advantage of this is that the simulators act just like the hardware in terms of how it interfaces with the support or flight equipment. The disadvantage is that the ability of the tester to inject faults into the system is compromised. The simulators could not be forced to report false information. For example, the only way an IRU simulator could report bad data is if the dynamics simulation reported incorrect data to the IRU. Thus the designer of a simulator must decide between increased ability to inject faults and a simulator that is more like the actual flight equipment.

A final lesson that applies not only to these simulators but to the laboratory environment as a whole is that in real time simulation, timing is everything. This was demonstrated with the RWA - RTIOU reset response simulation as well as the data transfers between the aspects of the simulators. Loss of data between the RWA simulator and mode] caused testing failures and the biggest problem with the support equipment software as a whole was data loss and corruption. Real time simulation is a great asset and an indispensable tool, but care must be taken to preserve data integrity to ensure consistent and reliable testing of subsystem hardware and software.

References

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Appendix A: Reaction Wheel Databus Transmission Decoding

In section 5.2.1, databus transactions revealed difficulties in simulating the reaction wheel's response to a remote terminal reset. This appendix shows how that data was decoded.

All transmissions on the AACS databus are known as packets. Commands from the AACS Flight Computer are denoted as reaction wheel destination packets since they come from the AFC and the destination is the reaction wheel. The designation for this packet is "bm_d_rwx2". This stands for bus monitor destination packet for reaction wheel electronics 2. There are two types of messages that the AFC sends to the reaction wheel-- commands and requests for data. A typical command packet is shown below. In the following explanations, a word is defined as four hexadecimal digits and a byte as 2 hexadecimal digits.

```
bm_d_rwx2=OOOeae040707 400100400665 CO 96
```

The first four hexadecimal digits (OOOe) are for support equipment processing and is not used by either the AFC or the RWA. The second "word" consists of two parts. Oxae denotes the address of the destination and stands for RWA2. 04 is a control byte that tells the RWA how to respond to the command. In this instance, 04 simply means that the packet is a command and is coming from the prime AFC. The third word tells the reaction wheel that the source was 07, which is AFC-A, and the number of bytes in this message is 7.

The commands start with OX40. The OX40 is a command to write data to a remote terminal address. Specifically, in this instance, it means to write one byte of data, starting at the address specified by the next byte. So, the 040100 is decoded to mean write one byte of data, starting at address 01, and that data is OX00. Register 01 of the reaction wheel's remote terminal is the torque enable command, so the AFC is enabling the RWA to accept the torque command.

The next command is similar. It reads 4006 65. This means to write one byte of data to the reaction wheel, starting at address 06, and that data is 0x65. This register is the torque command register. It is this register that we observed to fluctuate unexpectedly during the RWA RTIOU reset testing.

The final bytes are CO and 96. The OxCO is a “no operation” command and is needed to expand the packet to the correct length for the databus. The 96 is the checksum of the command,

A packet from the AFC to request data is similar to the command to write data:

bm_d_rwx2 = 0012 ae06070b 0002010300050006400400 10

The first three words have the same definitions as before. 0012 is used by the support equipment, ae06 says the destination is the RWA2 and the command is from the prime AFC (OX06 has identical meaning to 0x04), and 070b means the source is AFC-A and to expect 11 bytes in this packet (0x0b = 11 decimal).

The first command is OXOO02. This means collect one byte of data from address 02 (read to load RWA tachometer register). 0103 means collect two bytes starting at address 03 (upper and lower bytes of the tachometer). 0005 and 0006 decode to collect one word from registers 5 and 6 respectively (RWA line current and torque command wrap around). Finally, 040400 is a write of one byte to address 04 and that byte of data is OXOO. The Ox 10 is the checksum.

The second type of packet on the databus is from the RWA. This is denoted as bm_s_rwx2, meaning bus monitor source packet from reaction wheel electronics 2. A typical reply is shown below.

bm_s_rwx2 = 00100706 ae09 e00000 ff 000e 9165 CO 76

Again, the first word is for the support equipment, the second denotes the destination as 0x07 (AFC-A) and this time the OX06 is ignored, since the packet is not from the bus controller (AFC-A). ae09 decodes to mean the source is RWA2 and the number of bytes to expect is 9.

The first part of the reply is Oxe00000. In binary, this is three 1's followed by zeros. The three ones denote this packet as a reply and the zeros indicated no errors in this reply. Next comes the data in the order requested from the AFC. This packet was generated in response to the command to request data that was decoded earlier, so here is the data requested from registers 02 (0xff), 03 (0x00 0e), 05 (0x91) and 06 (0x65). Again, register six contains the torque command wrap-around that was observed to behave anomalously during testing. The CO is again the “no operation” command and the 76 is the checksum.

Appendix B: Source Code for software simulations

The following pages include the source code for the following models and simulations:

.Reaction Wheel Assembly Simulator

.Reaction Wheel Dynamics Model

.Engine Gimbal Actuator Dynamics Model

.Inertial Reference Unit Assembly Simulator

.Intertial Reference Unit Dynamics Model

100

```

period **/
**/
based on 400 Hz

based on 100 Hz

all angles

```

97/03/31
16:12:08

asm_iru.c

2

/** summation angles for a particular gyro **/

```
int      dyn_iru_rate[2][4];
int      angular_rate[2][4] = {0, 0, 0, 0, 0, 0, 0, 0};
int      dyn_rate_avail[2] = {0, 0};
int      internal_angular_rate[2][4];
int      Eangle[2][4];
double   DEangle[2][4];
int      iru_noise_index[2] = {0, 512};
int      iru_gyrosatr_delay[2][4];
double   iru_noise_array[1024] = {
-1.72614048501746E-06, 1.25455292857643E-06, 5.83641686687984E-07, 1.27800367515
740E-06,
1.48657820558932E-07, 1.31909572445318E-06, -3.52305310278122E-07, 1.97763345348
985E-06,
6.50103664136809E-07, -1.10545356321166E-06, 1.87654872197036E-06, 3.46774260010
270E-08,
-1.83212247943589E-06, -4.77664359071919E-07, -1.00944783752418E-06, -1.15449740
309575E-06,
-4.73929747008347E-07, 1.89942129338022E-06, -8.91091551437990E-07, -4.013854388
73152E-08,
6.79630415791694E-07, -3.63367265813063E-07, 1.67868110016987E-06, 1.2312015952
4139E-06,
-5.35845713222801E-07, 5.61465696601252E-07, -1.21746747604819E-06, 9.0161183643
0167E-08,
-1.45526869644867E-07, 1.10646012882237E-06, 1.47029802587954E-06, 5.170 5525500
4587E-08,
1.96625992694314E-06, -7.37128936772115E-07, -2.24485051447476E-09, 1.9935534270
6278E-06,
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67560E-07,
-1.92011834470616E-06, -1.07639035396707E-06, 1.10758721735874E-06, -6.54 9436880
91694E-07,
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3617E-07,
7.03725322816529E-07, 9.84766742425102E-07, -2.41149046046580E-07, 1.429 3402603
6167E-06,
-5.39531502721337E-07, -5.79355369052908E-07, 1.81998891117657E-06, 1.0439375258
0646E-06,
-1.75504180943286E-06, 5.36904124857416E-07, 4.59451538701734E-08, ..008.9872317
2915E-06,
2.88532885123957E-07, 4.74796760504963E-07, 7.09007763852420E-07, 5 888 809143466
01E-07,
1.45884119060671E-06, 6.31722766849071E-07, -1.82535161918240E-07, 1.536 8589841
2868E-06,
1.62154094216984E-06, -1.08010263792116E-06, 1.78328177877978E-06, 6.2921558560
0968E-07,
4.17275352453774E-07, -1.67405480833046E-06, -4.49952510210184E-07, 7.7 082175944
6483E-07,
-1.441048 64333 636E-06, 5.4296 8540261459E-08, 4.71921 876477766E-07, 1.81113556398
642E-06,
1.69315758125426 s-05, -1.43 2808918 67270E-06, 5.5200668395432 7E-07, -5.9939492325
444 8E-07,
1.8521526379300 3E-06, 5.5722 %653352391?-07, 1.0254 8087574458 E-06, -4.51517 %57405
592E-07,
-2.34773563 315680E-07, 1.9462 8405238477E-06, -5.8073141878 7649E-07, 2.54364 08925
22745-07,
1.3671667667 3693E-06, 2.3704 8937867921E-07, -1.3987447 8149150E-06, -1.4319018727
9782E-06,
1.78650428 165781E-06, 4.716 909638 85121E-07, 5.82747392627 838E-07, 1.25700574559?
40E-06,
8.54 898427733908E-07, 1.15032434074553 E-06, 1.4751909964743 8E-06, -1.10765149777
967E-07,
-2.449262105 PL7956E-07, -1.7 8001776541864E-0 5, 1.50177277611941 E-06, 7.9179230473
5794E-07,
```

```
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907524'2S-57,
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272?7222-0.5,
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87536834E-07,
7.8 80575562 795 69E-07, 1.9696037 5823138E- '25, -4.6261479932 875 0E-07, 1.8 855745
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5.2402759 8462745E-07, -5.53 984881403871E-07, -1.7537575145 8581E-06, -1.32074
373287554 E-06,
1.0195875 8815815E-06, -6.1911108444 9417E-07, 6.396559 94292808 E-07, 9.1592812
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551E-06,
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96142E-06,
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012E-0
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6193E-06,
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7600E-06,
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61E-07,
2.01190733014196E-06, 1.52618901938237E-06, -1.79083426931540E-06, 8.67213075833
907E-07,
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85216046E-06, -, 1.16566840536745E-06, -, 6.52324123446823E-07, 9.809630501411330E-07, -, 1.36364
205120807E-06, 1.35111768760645E-06, 4.170697046686053E-07, 3.37960240478444E-07, -, 1.6390359
0140774E-06, 7.08578411960828E-07, 1.84319131184423E-06, 1.40235552829100E-06, 6.3986282
5329641E-07, 6.6056441794058E-07, -, 1.05615044206538E-06, -, 1.05546262172385E-09, -, 9.42175
945696473E-08, -, 1.1670303021744430E-06, 5.21486998743170E-07, -, 1.379573316576796E-06, 1.907474
88388900E-06, 1.23700213083418E-06, 1.39129696101873E-06, -, 1.456055213342072E-06, 1.0765038
1511118E-07, -, 8.3189277831623E-07, 1.92021253057288E-06, -, 1.15827200238624E-06, -, 8.64929
011299081E-07, -, 9.61834281333590E-07, 1.01229290477067E-06, -, 1.56280391559527E-06, 1.390197
29641773E-06, 1.37665010175446E-06, 5.82839537942762E-07, -, 1.25665618770267E-06, 1.0639887
8798966E-06, -, 5.70231703408807E-07, -, 2.13705100976778E-08, 1.61436402418532E-06, -, 9.45697
503710589E-07, 2.315185695497327E-07, 3.92110983677179E-07, 1.31749135149351E-06, 1.85439445
508457E-06, 8.65547790091559E-07, 1.64296466753123E-06, -, 5.6528526456559E-07, 1.7202041
7134401E-06, -, 2.80581340372115E-07, 4.299336856806205E-07, 1.44864274400681E-06, -, 1.139177
36536217E-06, 1.53166161544967E-06, 1.31240798191820E-06, -, 1.31921363812076E-06, -, 2.63342
594037272E-08, 1.94291170779201E-06, 1.19425186236904E-06, -, 1.778649335032958E-06, 1.322157
80497720E-06, 3.49861255489330E-07, -, 2.62355573995900E-08, -, 1.23545034469329E-07, 1.70192
107799609E-06, 5.071166644896865E-07, -, 1.83125979343661E-06, 2.19209774181924E-07, 1.6669289
9519482E-06, 1.64263897576920E-06, 6.61066397618357E-07, 1.50650125921614E-06, 4.25638626
775617E-07, 1.52521292034018E-06, 1.97863920832445E-06, -, 6.00685358798245E-07, -, 1.287232



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48481058E-06,
-7.63119517406648E-07,-1.38703519677052E-06,1.28065404916377E-06,-9.32724665427880E-0
8);

```
/** Internal irq model data **/  
int last_irq_pwr[2] = {0, 0};  
int irq_mode[2] = {0, 0};  
float irq_timer[2] = {0, 0};  
int gyt_sat_mask[4] = {0x20, 0x10, 0x08, 0x04};  
int irq_hw4hz_cycle = 0;  
int irq_channel = 0;  
/** irq cycle execution array **/  
// In this array, the IRQ SIM will be executed if the value is not zero. **/  
// The ms cycle number was used, as opposed to just "1", so that the reader **/  
// will be able to easily located the desired slot number. Note: do not **/  
// use zero for slot zero because that will indicated not to be use the slot. **/  
// If zero needs to be used, cheat by inserting a "1". **/  
// This array is set up so that the irq is executed on the cycle before **/  
// the cycle where the data needs to be available. In this manner the **/  
// data will be available when the flight system accesses it. That of course **/  
// assumed that the flight system and the sim are synchronized which is **/  
// probably not the situation which then means that one does not care. **/  
// This scheme **/  
// was adopted because at 400 Hz there is not an integral number that **/  
// divides into 32768, the clock frequency. As a result any regular **/  
// update will begin to slide with respect to the rest of the system. **/  
int irq_cycle_array[1024] = {  
0, 1, 0, 0, 4, 0, 0, 6, 0, 0, 11, 0, 0, 14, 0,  
16, 0, 0, 19, 0, 0, 22, 0, 0, 24, 0, 0, 27, 0, 0,  
32, 0, 34, 0, 0, 37, 0, 0, 39, 0, 0, 42, 0, 0, 45, 0, 47,  
0, 0, 50, 0, 52, 0, 0, 55, 0, 0, 57, 0, 0, 60, 0, 0, 63,  
0, 65, 0, 0, 68, 0, 0, 70, 0, 0, 73, 0, 0, 75, 0, 0, 78, 0,  
80, 0, 0, 83, 0, 0, 86, 0, 0, 88, 0, 0, 91, 0, 0, 93, 0, 0,  
96, 0, 98, 0, 0, 101, 0, 0, 103, 0, 0, 106, 0, 0, 109, 0, 111,  
0, 0, 114, 0, 0, 116, 0, 0, 119, 0, 0, 121, 0, 0, 124, 0, 0, 127,  
0, 129, 0, 0, 132, 0, 134, 0, 0, 137, 0, 139, 0, 0, 142, 0,  
144, 0, 0, 147, 0, 0, 150, 0, 0, 152, 0, 0, 155, 0, 157, 0, 0,  
160, 0, 0, 162, 0, 0, 165, 0, 0, 167, 0, 0, 170, 0, 0, 173, 0, 0, 175,  
0, 0, 178, 0, 0, 180, 0, 0, 183, 0, 185, 0, 0, 188, 0, 0, 192,  
0, 193, 0, 0, 196, 0, 0, 201, 0, 203, 0, 0, 206, 0, 0,  
208, 0, 0, 211, 0, 0, 216, 0, 0, 219, 0, 0, 221, 0, 0,  
224, 0, 226, 0, 0, 229, 0, 231, 0, 0, 234, 0, 0, 237, 0, 239,  
0, 0, 242, 0, 244, 0, 0, 247, 0, 249, 0, 0, 252, 0, 0, 255,  
0, 257, 0, 0, 260, 0, 262, 0, 0, 265, 0, 267, 0, 0, 270, 0,  
272, 0, 0, 275, 0, 0, 278, 0, 280, 0, 0, 283, 0, 285, 0, 0,  
288, 0, 290, 0, 0, 293, 0, 0, 296, 0, 0, 301, 0, 303,  
0, 306, 0, 0, 308, 0, 311, 0, 313, 0, 0, 316, 0, 0, 319,  
0, 321, 0, 0, 324, 0, 326, 0, 0, 329, 0, 331, 0, 0, 334, 0,  
336, 0, 0, 339, 0, 0, 342, 0, 0, 344, 0, 0, 347, 0, 0, 349, 0, 0,  
352, 0, 0, 354, 0, 0, 357, 0, 0, 359, 0, 0, 362, 0, 0, 365, 0, 0, 367,  
0, 0, 370, 0, 0, 372, 0, 0, 375, 0, 377, 0, 0, 380, 0, 0, 383,  
0, 385, 0, 0, 388, 0, 390, 0, 0, 393, 0, 395, 0, 0, 398, 0, 0,  
400, 0, 0, 403, 0, 0, 406, 0, 0, 408, 0, 0, 411, 0, 413, 0, 0,  
416, 0, 418, 0, 0, 421, 0, 423, 0, 0, 426, 0, 0, 429, 0, 431,  
0, 0, 434, 0, 436, 0, 0, 439, 0, 441, 0, 0, 444, 0, 0, 447,  
449, 0, 0, 452, 0, 454, 0, 0, 457, 0, 459, 0, 0, 462, 0,  
464, 0, 0, 467, 0, 0, 470, 0, 0, 472, 0, 0, 475, 0, 0, 477, 0, 0,  
480, 0, 0, 482, 0, 0, 485, 0, 0, 487, 0, 0, 490, 0, 0, 493, 0, 0, 495,  
0, 0, 498, 0, 500, 0, 0, 503, 0, 505, 0, 0, 508, 0, 0, 511,  
0, 513, 0, 0, 516, 0, 518, 0, 0, 521, 0, 523, 0, 0, 526, 0,  
528, 0, 0, 531, 0, 0, 534, 0, 0, 536, 0, 0, 539, 0, 0, 541, 0, 0,  
544, 0, 0, 546, 0, 0, 549, 0, 0, 552, 0, 0, 554, 0, 0, 557, 0, 0, 559,  
0, 0, 562, 0, 564, 0, 0, 567, 0, 569, 0, 0, 572, 0, 0, 575,  
0, 577, 0, 0, 580, 0, 582, 0, 0, 585, 0, 587, 0, 0, 590, 0,  
592, 0, 0, 595, 0, 0, 598, 0, 0, 600, 0, 0, 603, 0, 605, 0, 0,  
608, 0, 610, 0, 0, 613, 0, 615, 0, 0, 618, 0, 0, 621, 0, 0, 623,  
0, 0, 626, 0, 628, 0, 0, 631, 0, 633, 0, 0, 636, 0, 0, 639,  
0, 641, 0, 0, 644, 0, 0, 646, 0, 0, 649, 0, 651, 0, 0, 654, 0,  
656, 0, 0, 659, 0, 0, 662, 0, 664, 0, 0, 667, 0, 0, 669, 0, 0,  
672, 0, 674, 0, 0, 677, 0, 679, 0, 0, 682, 0, 0, 685, 0, 0, 687,  
0, 0, 690, 0, 692, 0, 0, 695, 0, 697, 0, 0, 700, 0, 0, 703,  
0, 705, 0, 0, 708, 0, 710, 0, 0, 713, 0, 715, 0, 0, 718, 0,  
720, 0, 0, 723, 0, 0, 726, 0, 0, 728, 0, 0, 731, 0, 0, 733, 0, 0,  
736, 0, 0, 738, 0, 0, 741, 0, 743, 0, 0, 746, 0, 0, 749, 0, 0, 751,  
0, 0, 754, 0, 756, 0, 0, 759, 0, 761, 0, 0, 764, 0, 0, 767,  
0, 769, 0, 0, 772, 0, 774, 0, 0, 777, 0, 779, 0, 0, 782, 0,  
784, 0, 0, 787, 0, 0, 790, 0, 792, 0, 0, 795, 0, 797, 0, 0, 800,  
0, 0, 803, 0, 805, 0, 807, 0, 0, 810, 0, 0, 813, 0, 0, 815,  
0, 0, 818, 0, 820, 0, 0, 823, 0, 825, 0, 0, 828, 0, 0, 831,  
0, 833, 0, 0, 836, 0, 838, 0, 0, 841, 0, 843, 0, 0, 846, 0,  
849, 0, 0, 852, 0, 854, 0, 0, 856, 0, 0, 859, 0, 0, 861, 0, 0,  
864, 0, 0, 866, 0, 869, 0, 0, 871, 0, 0, 874, 0, 0, 877, 0, 0, 879,  
0, 0, 882, 0, 884, 0, 0, 887, 0, 889, 0, 0, 892, 0, 0, 895,  
0, 897, 0, 0, 900, 0, 902, 0, 0, 905, 0, 907, 0, 0, 910, 0,  
912, 0, 0, 915, 0, 918, 0, 0, 920, 0, 923, 0, 925, 0, 0, 928,  
0, 930, 0, 0, 933, 0, 935, 0, 938, 0, 0, 941, 0, 943,  
946, 0, 0, 948, 0, 951, 0, 953, 0, 956, 0, 0, 959,  
961, 0, 0, 964, 0, 966, 0, 0, 969, 0, 971, 0, 0, 974, 0,  
976, 0, 0, 979, 0, 982, 0, 984, 0, 0, 987, 0, 989, 0, 0, 992,  
994, 0, 0, 997, 0, 999, 0, 0, 1002, 0, 0, 1005, 0, 1007,  
1010, 0, 1012, 0, 1015, 0, 1017, 0, 0, 1020, 0, 0, 1023};  
/** Test visibility data for debugging purposes **/  
int dim_gyr_stra = 0;  
int dim_gyr_strb = 0;  
int trap_angular_rate_a;  
int trap_angular_rate_b;  
int trap_angular_rate_c;  
int trap_angular_rate_d;  
int trap_i;  
int trap_mask;  
double trap_angle_rate;  
int soft_reset_flag[2] = {0, 0};  
int dwn_ld_done[2] = {0, 0};  
int funcodaa;  
int funcodebb;  
int mspacea;  
int mspaceb;  
/** unused parameters, can these be deleted? **/  
RING_ID irq_ring_0 = 0;  
int irq_task_id = 0;  
int irq_0_task();  
/** irq model code **/  
int irq_reset(irq_device_id)  
int irq_device_id; // irq_a = 0, irq_b = 1 */
```


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```
/* mark data according to computed valid bits */
poke8(assem_iirub + (0x10 << 1) + 1, iiru_datavalid(0));

if (out & 0x000f) != 0 {
}
};
};

if (id == 1 && (assem_iirub_write_ok == 1) || (afc == 0)) {
    * OK to write to assembly unit, if the flight computer
    * starts a transaction while in this block, we should be
    * able to finish before the assembly unit actually responds
    * to the read but we will protect ourselves by marking the
    * data invalid during the write process
    */
    /* poke8(assem_iirub + (0x10 << 1) + 1, iiru_datainvalid); */

    if (out & 0x0010) != 0 {
        poke8(assem_iirub + (0x11 << 1) + 1, iiru_gyrosatr(1));
        poke8(assem_iirub + (0x1e << 1) + 1, iiru_timetag1_idl);
        poke8(assem_iirub + (0x1f << 1) + 1, iiru_timetag0_idl);
        poke8(assem_iirub + (0x20 << 1) + 1, bit_stat[id]);
        poke8(assem_iirub + (0x21 << 1) + 1, bit_crn1[id]);
        poke8(assem_iirub + (0x2a << 1) + 1, bit_cpu0[id]);
        poke8(assem_iirub + (0x2b << 1) + 1, bit_cpu0[id]);
        poke8(assem_iirub + (0x2c << 1) + 1, bit_psm1[id]);
        poke8(assem_iirub + (0x2d << 1) + 1, bit_psm0[id]);
        poke8(assem_iirub + (0x2e << 1) + 1, bit_dnld[id]);
    }

    if (out & 0x0008) != 0 {
        poke8(assem_iirub + (0x12 << 1) + 1, gyroB_angle_A2);
        poke8(assem_iirub + (0x13 << 1) + 1, gyroB_angle_A1);
        poke8(assem_iirub + (0x14 << 1) + 1, gyroB_angle_A0);
        poke8(assem_iirub + (0x22 << 1) + 1, bitgyr1[id]);
        poke8(assem_iirub + (0x23 << 1) + 1, bitgyra0[id]);
    }

    if (out & 0x0004) != 0 {
        poke8(assem_iirub + (0x15 << 1) + 1, gyroB_angle_B2);
        poke8(assem_iirub + (0x16 << 1) + 1, gyroB_angle_B1);
        poke8(assem_iirub + (0x17 << 1) + 1, gyroB_angle_B0);
        poke8(assem_iirub + (0x24 << 1) + 1, bitgyrb1[id]);
        poke8(assem_iirub + (0x25 << 1) + 1, bitgyrb0[id]);
    }

    if ((out & 0x0002) != 0) {
        poke8(assem_iirub + (0x18 << 1) + 1, gyroB_angle_C2);
        poke8(assem_iirub + (0x19 << 1) + 1, gyroB_angle_C1);
        poke8(assem_iirub + (0x1a << 1) + 1, gyroB_angle_C0);
        poke8(assem_iirub + (0x26 << 1) + 1, bitgyrc1[id]);
        poke8(assem_iirub + (0x27 << 1) + 1, bitgyrc0[id]);
    }

    if (out & 0x0001) != 0 {
        poke8(assem_iirub + (0x1b << 1) + 1, gyroB_angle_D2);
        poke8(assem_iirub + (0x1c << 1) + 1, gyroB_angle_D1);
        poke8(assem_iirub + (0x1d << 1) + 1, gyroB_angle_D0);
        poke8(assem_iirub + (0x28 << 1) + 1, bitgyrd1[id]);
        poke8(assem_iirub + (0x29 << 1) + 1, bitgyrd0[id]);
    }

    /* mark data according to computed valid bits */
    poke8(assem_iirub + (0x10 << 1) + 1, iiru_datavalid(1));
}

if ((out & 0x000f) != 0) {
    /* indicate data written not just status words */
    card[id].assem_write_done = 1;
}

double
iiru_noise(i)
int i;
{
    iiru_noise_index[i] = ++iiru_noise_index[i] & 0x03ff;
    return (iiru_noise_array[iiru_noise_index[i]]);
}

int
update_time(i)
int i;
{
    unsigned short int TIMETAG;
    /**
     * Calculate IRU time TIMETAG1 and TIMETAG0
     */
    iiru_timetag[i] = iiru_timetag[i] + iiru_cycle_time;
    if (iiru_timetag[i] > iiru_timetag_rollover) {
        /* we have bits to spare so ">" vs ">=" does not matter */
        iiru_timetag[i] -= iiru_timetag_rollover;
    }
    /**
     * TIMETAG = (iiru_timetag[i] / 1000.0) * 1.0e6;
     */
    TIMETAG = iiru_timetag[i] / iiru_timetag_sf;
    return (TIMETAG);
}

int
read_iiru_power(base)
char *base
{
    int pwr_status;

    pwr_status = peek8(base + 0x8000 + 1);
    return (pwr_status);
}

int
reset_board(base)
char *base
{
    int dummy;

    dummy = poke(base + (0x8002 + 1) + 0x0e);
    /* data is don't care */
}
```


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```
return (0) ;

};

int
check_status_register (board)
    int         board;

{
    card [board].pwr = read_iru_power ( *card [board].base_addr ) ;

    cardboard [board].assem_RTIOU_ct--;

    if ( ( (card [board].last_pwr & 0x04) == 0x00) && ( (cardboard [board].pwr & 0x04) != 0x00) ) {
        /* device just turned on  send reset */
        reset_board ( *card [board].base_addr ) ;
    }

    if ((card [board].pwr & 0x04) == 0x00) {
        card [board].assem_insync = 0 ;
        cardboard [board].assem_RTIOU_ct = cardboard [board].RTIOU_reset_limit;
        card [board].consecutive_recycles = 0 ;
    }

    if ( ( (card [board].last_pwr & 0x08) == 0) && ((card [board].pwr & 0x08) != 0) ) {
        /* AFC has started an assembly card transaction */
        card [board].assem_RTIOU_int_pt = cardboard [board].assem_RTIOU_ct ;
        if (cardboard [board].assem_write_ok == 1) {
            /* AFC transaction occurred when writes not inhibited */
            card [board].assem_possible_parity_ct++;
            checkpoint_2_card [board] = card [board];
        }
    }

    if ( ( (card [board].last_pwr & 0x08) != 0) && ((card [board].pwr & 0x08) == 0) ) {
        /* AFC has completed an assembly card transaction */
        checkpoint_2_card [board] = cardboard ;
        if ( (cardboard [board].assem_RTIOU_ct < card [board].RTIOU_lockout_value) &
            (card [board].consecutive_recycles > cardboard [board].consecutive_recycles
            _limit)) {
            /*
             * if we have recycled, ie assem_RTIOU_ct is near
             * RTIOU_reset_limit not 0, do not reset - assume we
             * are in sync but count consecutive misses after
             * limit resync to signal
             */
            card [board].assem_RTIOU_ct = card [board].RTIOU_reset_limit;
            cardboard [board].consecutive_recycles = 0;
        } else {
            cardboard [board].consecutive_recycles++;
        }
        card [board].assem_insync = 1 ;
        cardboard [board].assem_write_done = 0 ;          /* allow another write
                                                             * at proper time */
        card [board].assem_int_active++;
    }

    card [board].last_pwr = cardboard [board].pwr;

    if (card [board].assem_RTIOU_ct < card [board].RTIOU_recycle_value) {
        /*
         * either interrupts are off, or assem card not read, reset
         * counter and disable interrupt
         */
        cardboard [board].assem_RTIOU_ct = card [board].RTIOU_reset_limit;
        card [board].assem_sync_loss_ct++;
        card [board].assem_write_done = 0 ;              /* allow another write
                                                             * at proper time */

        /* card [board].assem_insync = 0; */
        /* poke8 (*card [board].base_addr + 0x8006 + 1, 0xee) ; */
    }

    if ( (cardboard [board].assem_RTIOU_ct > card [board].RTIOU_interrupt_enable_value)
        && (card [board].assem_RTIOU_ct < card [board].RTIOU_lockout_value) &
        (card [board].assem_write_done != 0) &&
        (card [board].assem_insync == 0) ) {
        card [board].assem_write_ok = 0 ; /* inhibit writes */
    } else {
        cardboard [board].assem_write_ok = 1 ; /* enable writes */
    }

    return 0;
}

int
check_iru_status_register ()
{
    iru_pwr [0] = read_iru_power ( assem_irua ) ;
    iru_pwr [1] = read_iru_power ( assem_irub ) ;

    if (((last_iru_pwr [0] & 0x08) == 0) && ((iru_pwr [0] & 0x08) != 0)) {
        /* AFC has started an assembly card transaction */
        assem_irua_RTIOU_int_pt = assem_irua_RTIOU_ct ;
        if (assem_irua_write_ok == 1) {
            /* AFC transaction occurred when writes not inhibited */
            assem_irua_possible_parity_ct++;
        }
    }

    if (((last_iru_pwr [0] & 0x08) != 0) && ((iru_pwr [0] & 0x08) == 0)) {
        /* AFC has completed an assembly card transaction */
        assem_irua_RTIOU_ct = iru_RTIOU_reset_limit;
        assem_irua_insync = 1 ;
        assem_irua_int_active++;
    }

    if ( ( (last_iru_pwr [1] & 0x08) == 0) && ((iru_pwr [1] & 0x08) != 0) ) {
        /* AFC has started an assembly card Transaction. */
        assem_irub_RTIOU_int_pt = assem_irub_RTIOU_ct;
        if (assem_irub_write_ok == 1) {
            /* AFC transaction occurred when writes not inhibited */
            assem_irub_possible_parity_ct++;
        }
    }

    if (((last_iru_pwr [1] & 0x08) != 0) && ((iru_pwr [1] & 0x08) == 0)) {
        /* AFC has completed an assembly card transaction */
        assem_irub_RTIOU_ct = iru_RTIOU_reset_limit;
        assem_irub_insync = 1 ;
        assem_irub_int_active++;
    }

    last_iru_pwr [0] = iru_pwr [0] ;
    last_iru_pwr [1] = iru_pwr [1] ;
}
```

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```
if ( assem_i rua_RTIOU_ct-- < iru_RTIOU_recycle_value ) (
/*
    *either interrupts are off, or assem card not read, reset
    * counter and disable interrupt
    */
    assem_i rua_RTIOU_ct = iru_RTIOU_reset_limit;
    assem_i rua_syncloss_ct++;
    /* assem_irua_insync = 0; */
    /* poke8(assem_irua + 0x8006 + 1, 0xee); */
);
if ( assem_i rub_RTIOU_ct-- < iru_RTIOU_recycle_value ) {
/*
    * either interrupts are off, or assem card not read, reset
    * counter and disable interrupt
    */
    assem_irub_RTIOU_ct = iru_RTIOU_reset_limit;
    assem_i rub_syncloss_ct++;
    /* assem_irub_insync = 0; */
    /* poke8(assem_irub + 0x8006 + 1, 0xee); */
};

if ( ( assem_irua_RTIOU_ct > iru_RTIOU_interrupt_enable_value ) &
    ( assem_i rua_RTIOU_ct < iru_RTIOU_lockout_value ) &
    ( assem_irua_insync == C ) ) {
    assem_irua_write_ok = 0;          /* inhibit writes */
} else {
    assem_irua_write_ok = 1;          /* enable writes */
};

if ( ( assem_irub_RTIOU_ct > iru_RTIOU_interrupt_enable_value ) &
    ( assem_i rub_RTIOU_ct < iru_RTIOU_lockout_value ) &
    ( assem_irub_insync == C ) ) {
    assem_i rub_write_ok = 0;          /* inhibit writes */
} else {
    assem_i rub_write_ok = 1;          /* enable writes */
};

return 0;
};

int
iru_integrator ( )
{
    int            i, j;

    for ( i = 0; i < 6; i++ ) {
        check_status_register ! i ;
    };

    iru_1024_hz_cycle++;
    iru_1024_hz_cycle = iru_1024_hz_cycle & 0x000003ff;

    if (iru_cycle_array[iru_1024_hz_cycle] != 0) {
        iru_channel = (iru_channel + 1) & 0x00000003;
        iru_sim ( iru_channel );
    } else {
        if (iru_channel == 3) { /** safe to pick up dynamics rates */
            for ( i = 0; i < 2; i++ ) {
                if (dyn_rate_avail[i] != 0) {
                    for ( j = 0; j < 4; j++ ) {
                        angular_rate[i][j] = dyn_iru_rate[i][j];
                    };
                    dyn_rate_avail[i] = 0;
                };
            };
        };
    };
};

int
iru_sum_angle ( id, i )
int            id;
int            i;
```

```
};
return 0;
};

int
iru_sum_angle ( id, i )
int            id;
int            i;

double          angle_rate;
unsigned short int time;

if ( i == 0 ) {          /** time and sat. bits are synced to start of update cycle */
    iru_gyrosatr[id] = 0x00;          /* clear saturation bits */
    time = update_time(id);
    iru_tmetag0[id] = time & 0x00ff;
    iru_tmetag1[id] = time >> 8;

    angle_rate = angular_rate[id][i];

    /**
    ** if angular rate exceeds 15 deg/sec set corresponding
    ** gyro saturation bit
    */

    if (fabs(angle_rate) > (scaled_iru_gyro_sat_limit) ) {
        if (id == 0) {
            Jim_gyr_stra++;
        } else {
            Jim_gyr_strb++;

            iru_gyrosatr[id] = iru_gyrosatr[id] | gyro_sat_mask[i];
            DEangle[id][i] = 0.0;          /** set integrated angle to 0 */
            iru_gyrosatr_delay[id][i] = iru_gyrosatr_delay_time;
            trap_angular_rate_a = angular_rate[id][0];
            trap_angular_rate_b = angular_rate[id][1];
            trap_angular_rate_c = angular_rate[id][2];
            trap_angular_rate_d = angular_rate[id][3];
            trap_i = i;
            trap_mask = iru_gyrosatr[id];
            trap_angle_rate = angle_rate;
        } else {
            if ( (--iru_gyrosatr_delay[id][i]) <= 0 ) {
                iru_gyrosatr_delay[id][i] = 0;
                /** apply cycle delta time and scale factor */
                DEangle[id][i] += (angle_rate * iru_cycle_time_sf);
                if (DEangle[id][i] >= iru_rollover) {
                    DEangle[id][i] -= iru_rollover;
                } else {
                    if (DEangle[id][i] <= -iru_rollover) {
                        DEangle[id][i] += iru_rollover;
                    }
                }
            } else {
                /** keepsat flag condition until timer expires */
                iru_gyrosatr[id] = iru_gyrosatr[id] | gyro_sat_mask[i];
                DEangle[id][i] = 0.0;          /** set integrated angle to 0 */
            };
        };
    };
    if ( (iru_noise_on != 0) && ( (iru_gyrosatr[id] & gyro_sat_mask[i]) == 0 ) )
        DEangle[id][i] = (DEangle[id][i] + iru_noise(id)) / iru_angle_sf;
    else
```

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```
Eangle[id][i] = DEangle[id][i] / iru_angle_sf;

iru_datavalid[id] = 0x00bc ^ iru_gyrosatr[id]; /** bit 7 always = 1 **/

if(id == 0) {

    switch (i) {

    case 0:
        gyroA_angle_A0 = Eangle[id][0] & 0x000000ff;
        gyroA_angle_A1 = (Eangle[id][0] >> 8) & 0x000000ff;
        gyroA_angle_A2 = (Eangle[id][0] >> 16) & 0x000000ff;
        break;

    case 1:
        gyroA_angle_B0 = Eangle[id][1] & 0x000000ff;
        gyroA_angle_B1 = (Eangle[id][1] >> 8) & 0x000000ff;
        gyroA_angle_B2 = (Eangle[id][1] >> 16) & 0x000000ff;
        break;

    case 2:
        gyroA_angle_C0 = Eangle[id][2] & 0x000000ff;
        gyroA_angle_C1 = (Eangle[id][2] >> 8) & 0x000000ff;
        gyroA_angle_C2 = (Eangle[id][2] >> 16) & 0x000000ff;
        break;

    case 3:
        gyroA_angle_D0 = Eangle[id][3] & 0x000000ff;
        gyroA_angle_D1 = (Eangle[id][3] >> 8) & 0x000000ff;
        gyroA_angle_D2 = (Eangle[id][3] >> 16) & 0x000000ff;
        break;

    },

};

if (id == 1) {

    switch (i) {

    case 0:
        gyroB_angle_A0 = Eangle[id][0] & 0x000000ff;
        gyroB_angle_A1 = (Eangle[id][0] >> 8) & 0x000000ff;
        gyroB_angle_A2 = (Eangle[id][0] >> 16) & 0x000000ff;
        break;

    case 1:
        gyroB_angle_B0 = Eangle[id][1] & 0x000000ff;
        gyroB_angle_B1 = (Eangle[id][1] >> 8) & 0x000000ff;
        gyroB_angle_B2 = (Eangle[id][1] >> 16) & 0x000000ff;
        break;

    case 2:
        gyroB_angle_C0 = Eangle[id][2] & 0x000000ff;
        gyroB_angle_C1 = (Eangle[id][2] >> 8) & 0x000000ff;
        gyroB_angle_C2 = (Eangle[id][2] >> 16) & 0x000000ff;
        break;

    case 3:
        gyroB_angle_D0 = Eangle[id][3] & 0x000000ff;
        gyroB_angle_D1 = (Eangle[id][3] >> 8) & 0x000000ff;
        gyroB_angle_D2 = (Eangle[id][3] >> 16) & 0x000000ff;
        break;

    },

};
```

```
};

int
iru_sim ( target_channel )
{
    int t_channel; /* 0=chan A, 1=chan B, 2.than C, 3.than D */

    /*
    {

    int i;
    int SftRst[2]; /** Soft Reset Function code **/
    /**int angular_rate[2][4]; **/
    /** iru_mode: 0 = power off to on transition,
    1 = power turned on - doing BIT 1 sec timer,
    2 = wait for download to complete,
    3 = soft reset,
    4 = normal **/

    SftRst[0] = peek8(assem_irua + (0x80 << 1) + 1);

    if ((SftRst[0] != 0x03) ||
        (peek8(assem_irua + (0x81 << 1) + 1) != 0x00) ||
        (peek8(assem_irua + (0x82 << 1) + 1) != 0x00) ||
        (peek8(assem_irua + (0x83 << 1) + 1) != 0x00) ||
        (peek8(assem_irua + (0x84 << 1) + 1) != 0x00) ||
        (peek8(assem_irua + (0x85 << 1) + 1) != 0x00) ||
        (peek8(assem_irua + (0x86 << 1) + 1) != 0x00) ) {
        /* die? not pass reset packet test */

        SftRst[0] = 0;

    };

    SftRst[1] = peek8(assem_irub + (0x80 << 1) + 1);

    if ((SftRst[1] != 0x03) ||
        (peek8(assem_irub + (0x81 << 1) + 1) != 0x00) ||
        (peek8(assem_irub + (0x82 << 1) + 1) != 0x00) ||
        (peek8(assem_irub + (0x83 << 1) + 1) != 0x00) ||
        (peek8(assem_irub + (0x84 << 1) + 1) != 0x00) ||
        (peek8(assem_irub + (0x85 << 1) + 1) != 0x00) ||
        (peek8(assem_irub + (0x86 << 1) + 1) != 0x00) ) {
        /* did not pass reset packet test */
        SftRst[1] = 0;

    };

    for (i = 0; i < 2; i++) {

        if ((card[i].pwr & 0x04) == 0) { /** device is off **/
            iru_reset(i);
            bit_crnt[i] = 0x00;
            bit_dnld[i] = 0x00;
            dwm_ld_done[i] = 0x00;
            iru_mode[i] = 0;
        } else { /** device is on **/

            switch (iru_mode[i]) {

            case 0: /** device just turned on **/
                iru_reset(i);
                iru_rtiou_write(i, 31, force_write); /** initiali
```

ze iru data **/

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```
/**/
    iru_timer[i] = iru_BIT_time;    /** counts down to zero
    iru_mode[i] = 1;
    break;

case 1: /** 1 second BIT timer */
    if (iru_timer[i] > 0) {
        iru_timer[i]--;
    } else {    /** timer expired */

        bit_dnld[i] = 0x30;    /** BIT complete */
        iru_gyrostatr[i] = 0x00;
        bit_crnt[i] = 500 / 15.625;
        dwn_ld_done[i] = 0x05;
        iru_rtiou_write(i, 16, force_write);    /** update status only */

        iru_mode[i] = 2;
    };
    break;

case 2: /** wait for download to complete */

    /** check for soft reset */
    if (SftRst[i] == 0x03) !    /** soft reset just occurred */

        iru_reset(i);
        iru_rtiou_write(i, 31, force_write)    /** update all */
        iru_timer[i] = iru_soft_reset_time;    /** counts down to zero */
        iru_mode[i] = 3;
    } else !

        if (dwn_ld_done[i] == 0x0f) {    /** download complete */

            iru_mode[i] = 4;
            ! else {    /** check for download complete */

                iru_download(i);
            }
        };
        break;

case 3: /** soft reset delay 1 second timer */
    if (iru_timer[i] > 0) !
        iru_timer[i]--;
    ! else {    /** timer expired */

        /**
        ** this prevents a continuous soft reset
        ** by writing over the function code
        */

        if (i == 0) {
            poke8(assem_irua + (0x80 << 1) + 1, 0xff);
        };

        if (i == 1) {
            poke8(assem_irub + (0x80 << 1) + 1, 0xff);
        };
    };

    iru_rtiou_write(i, 15, force_write);    /**
    soft_reset_flag[i] = 1;

    if (dwn_ld_done[i] == 0x0f) {    /** download
        iru_mode[i] = 4;
        ? else !    /** check for download complete
            iru_mode[i] = 2;
        };
        break;

case 4: /** normal operation */

    /** check for soft reset first before calculating angles */
    if (SftRst[i] == 0x03) {    /** soft reset just
        iru_reset(i);
        iru_rtiou_write(i, 31, force_write);    /**
        iru_timer[i] = iru_soft_reset_time;    /**
        iru_mode[i] = 3;
    } else {
        iru_sum_angle(i, target_channel);
        if (target_channel == 3) !
            /** write to iru after all angles complete */
            iru_rtiou_write(i, 31, check_afc);
        };
        break;
    };

    if (iru_mode[i] != 4) !
        card[i].assem_insic = 0;
    };

};

int
iru_download(id)
    int
        id;

    if ((id == 0) && (fake_download != 1)) {
        FuncCodeA = peek8(assem_irua + (0x80 << 1) + 1);
        if (FuncCodeA == 0x09) !
            MspaceA = peek8(assem_irua + (0x80 << 1) + 5);
            if (MspaceA == 0x00) !
                /** 0x00 space GSP p-space */
                bit_dnld[id] = bit_dnld[id] ! 0xc0;
                poke8(assem_irua + (0x2e << 1) + 1, bit_dnld[id] ! ;
                /** checksum on p-space good */
            };
        };
    };
};
```

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```
        dwn_ld_done[id] = dwn_ld_done[id] | 0x03 ;
    };

    if (MspaceA == 0x10) {
        /* 0x00 space d-space */
        bit_dnld[id] = bit_dnld[id] ^ 0x0c;
        poke8(assem_irua + (0x2e << 1) + 1, bit_dnld[id] );
        /* chksum on d-space good */
        dwn_ld_done[id] = dwn_ld_done[id] ^ 0x0c;
    };

};

};

if ((id == 1) && (fake_download != 1)) {

    Func Code B = peek 8 (assem_irub + (0x80 << 1) . 1) ;

    if (Fix.cCode2 == 0x09 ) {
        Mspace B = peek8 (assem_irub . (0x80 << 1) + 5 ) ;
        if (MspaceB == 0x00) !
            /* 0x00 space GSPp-space */
            bit_dnld[id] = bit_dnld[id] ^ 0xc0;
            poke8 (assem_irub + (0x2e << 1) + 1, bit_dnld[id] ) ;
            /* chksum on p-space good */
            dwn_ld_done[id] = dwn_ld_done[id] ^ 0x03 ;
        };

        if (MspaceB == 0x10) {
            /* 0x00 space d-space */
            bit_dnld[id] = bit_dnld[id] ^ 0x0c;
            poke8 (assem_irub + (0x2e << 1) + 1, bit_dnld[id]);
            /* chksum on d-space good */
            dwn_ld_done[id] = dwn_ld_done[id] ^ 0x0c;
        };

    },

    if (fake_download == 1) {
        bit_dnld[id] = 0xfc;
        iru_datavalid[id] = 0xbc;
        dwn_ld_done[id] = 0xf;
    };

}

int
run_assem()
{
    rwa_loop ();
    return 0;
}
```

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ega_model.c

```
/* ega_model.c */
/* cassinini iti ega model */

/* for the d_real typedef */
#include "types-darts.h"

/* for matrix subroutines */
#include "linalg-darts.h"

/* standard */
#include <string.h>

/* local */
#include "ega_model.h"

/* Diagnostics */
extern int model;
extern int diag_time;
extern int diag_level;
extern FILE *f_ega;
extern int diag_flag;
extern d_real bb_tinmetag

/* local functions */
void ega_kinematics(), ega_extension(), l2solve()

/* namelist data */
d_real ega_max_delta, ndlvlvt, ega_null_length, ega_err_tol, p_joint[2][2][3], u
_joint[2][2][3], me2_null_trans[3][3], me1_null_trans[3][3];

int ega_counter_max;

/* local to model */
d_real ega_curr_ext[4];
int ega_onoff_a, ega_onoff_b;

/** Modification 29 July 96 J. Bunn:
Changed onoff_a(b) to ega_onoff_a(b) to avoid model conflicts
Changed default to ON
**/

void ega_init
{
    int i

    /* namelist parameters */

    ega_null_length = 9.8;
    ega_max_delta = 0.0667;
    ega_max_delta = 0.01;
    ndlvlvt = 4.;

    /* me1_null_trans are the transformations from engine to spacecraft
    * coords
    */
    me1_null_trans[0][0] = 0.99863117108034;
    me1_null_trans[0][1] = 0.00000000000000;
    me1_null_trans[0][2] = -0.05230472394256
    me1_null_trans[1][0] = 0.00496283907661;
    me1_null_trans[1][1] = 0.99548841288797;
    me1_null_trans[1][2] = 0.09475331146768;
    me1_null_trans[2][0] = 0.05206874662412;

    me2_null_trans[0][0] = 0.99863792821450;
    me2_null_trans[0][1] = 0.00000000000000;
    me2_null_trans[0][2] = -0.0521755300558;
    me2_null_trans[1][0] = -0.00615247411855;
    me2_null_trans[1][1] = 0.99302325091709;
    me2_null_trans[1][2] = -0.1177581003948;
    me2_null_trans[2][0] = 0.05181153726400;
    me2_null_trans[2][1] = 0.11791871411295;
    me2_null_trans[2][2] = 0.99167068196467;

    ega_err_tol = 1.e-7;
    ega_counter_max = 5;

    /* REA-1 */
    p_joint[0][0][0] = 0.09826216260427;
    p_joint[0][0][1] = 0.19326857152374;
    p_joint[0][0][2] = -0.24259124338664;
    p_joint[0][1][0] = -0.09700628079466;
    p_joint[0][1][1] = 0.19342412374100;
    p_joint[0][1][2] = -0.24261331226352;
    p_joint[0][2][0] = 0.77279074868430;
    p_joint[0][2][1] = -0.4847569251892;
    p_joint[0][2][2] = -0.53457785616215;
    p_joint[0][3][0] = -0.77526482865983;
    p_joint[0][3][1] = -0.48079894849746;
    p_joint[0][3][2] = -0.53492556383186;

    /* REA-2 */
    p_joint[1][0][0] = 0.09952277331660;
    p_joint[1][0][1] = -0.19265782170509;
    p_joint[1][0][2] = -0.24251971359319;
    p_joint[1][1][0] = -0.09493540852512;
    p_joint[1][1][1] = -0.19306247519653;
    p_joint[1][1][2] = -0.24270448158418;
    p_joint[1][2][0] = 0.76977251224720;
    p_joint[1][2][1] = 0.48934508284425;
    p_joint[1][2][2] = -0.53489852290059;
    p_joint[1][3][0] = -0.77823654184649;
    p_joint[1][3][1] = 0.47609528989577;
    p_joint[1][3][2] = -0.53455712336594;

    /* initialize */
    for (i = 0; i < 4; i++)
        ega_curr_ext[i] = 0.;

    /* default on */
    ega_onoff_a = 1;
    ega_onoff_b = 1;
}

void ega_onoff(onoff_str)
    char onoff_str[]
{
    if ( strcmp(onoff_str, "egaa on") )
        ega_onoff_a = 1;
    if ( strcmp(onoff_str, "egaa off") )
        ega_onoff_a = 0;
    if ( strcmp(onoff_str, "egab on") )
        ega_onoff_b = 1;
    if ( strcmp(onoff_str, "egab off") )
        ega_onoff_b = 0;
}
```

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ega_model.c

```

)

/*
 * Indexing: ((+Y REA/+X EGA), ((+Y REA/-X EGA), (-Y ? EA/+X EGA), (-Y P. EA/-X
 * EGA))
 *
 * Note that within the CAB documentation, the +Y REA is designate? as the A REA
 * and the -Y REA is designated as the B REA. Additionally, the +X EGA is
 * designated as EGAPA, while the -X EGA is designated as EGAQA.
 *
 * me1_u_vec: Unit vector of +Y ME thrust in S/C coords me2_u_vec: Unit
 * vector of -Y ME thrust in S/C coords
 */

void
ega_model ( ega_ext_com, lvd_t_pos_est, me1_u_vec, me2_u_vec )
    d_real      ega_ext_com[], lvd_t_pos_est[], me1_u_vec[], me2_u_vec[];

/*
 * in:  ega_ext_com  commanded extensions lvd_t_pos_est lvd_t extensions
 *
 * out: me1_u_vec   main engine vectors me2_u_vec
 */

{
    d_real      delta;
    int          i;

    if (ega_onoff_a) {

        /* update state per command -- limit if necessary: */
        for (i = 0; i < 2; i++) {
            ega_ext_com[i * 2 + 0] = ega_ext_com[i * 2 + 0] * .00027246;
            lvd_t_pos_est[i * 2 + 0] = lvd_t_pos_est[i * 2 + 0] * .00027246;
            delta = ega_ext_com[i * 2 + 0] - ega_curr_ext[i * 2 + 0];
            if (delta > ega_max_delta)
                ega_curr_ext[i * 2 + 0] += ega_max_delta;
            else if (delta < -ega_max_delta)
                ega_curr_ext[i * 2 + 0] -= ega_max_delta;
            else
                ega_curr_ext[i * 2 + 0] = ega_ext_com[i * 2 + 0];

            /* check lvd_t data */
            for (i = 0; i < 2; i++) {
                if (fabs(lvd_t_pos_est[i * 2 + 0] - ega_curr_ext[i * 2 + 0]) > nd
                    lvd_t * ega_max_delta)
                    ega_curr_ext[i * 2 + 0] = lvd_t_pos_est[i * 2 + 0];
            }

            if (ega_onoff_b) {

                /* update state per command -- limit if necessary: */
                for (i = 0; i < 2; i++) {
                    ega_ext_com[i * 2 + 1] = ega_ext_com[i * 2 + 1] * .00027246;
                    lvd_t_pos_est[i * 2 + 1] = lvd_t_pos_est[i * 2 + 1] * .00027246;
                    delta = ega_ext_com[i * 2 + 1] - ega_curr_ext[i * 2 + 1];
                    if (delta > ega_max_delta)
                        ega_curr_ext[i * 2 + 1] += ega_max_delta;
                    else if (delta < -ega_max_delta)
                        ega_curr_ext[i * 2 + 1] -= ega_max_delta;
                    else
                        ega_curr_ext[i * 2 + 1] = ega_ext_com[i * 2 + 1];
                }
            }
        }

        /* check lvd_t data */
        for (i = 0; i < 2; i++) {
            if (fabs(lvd_t_pos_est[i * 2 + 1] - ega_curr_ext[i * 2 + 1]) > nd
                lvd_t * ega_max_delta)
                ega_curr_ext[i * 2 + 1] = lvd_t_pos_est[i * 2 + 1];
        }
    }

    /* kinematics */
    ega_kinematics(me1_u_vec, me2_u_vec);

    /* Diagnostics */
    if (model == 3 && diag_time - > 0) {
        if (diag_flag == 0) {
            if ((f_ega = fopen("/si m/tmp/ega_diags", "w")) == (FILE *)
                ULL) {
                printf("File Open Load Failure for EGA diagnostics\n");
            }
            diag_flag = 1;
        }
        if (diag_level == 1 || diag_level == 2 || diag_level == 3) {
            if (f_ega == (FILE *) NULL) {
                printf("OUTPUTS: me1_u_vec %12.6f %12.6f %12.6f\n",
                    me2_u_vec[0], me2_u_vec[1], me2_u_vec[2]);
            } else {
                fprintf(f_ega, "OUTPUTS: me1_u_vec %12.6f %12.6f %12.6f\n",
                    me2_u_vec[0], me2_u_vec[1], me2_u_vec[2]);
            }
        }
        if (diag_level == 2 || diag_level == 3) {
            if (f_ega == (FILE *) NULL) {
                printf("INPUTS: Est. Com: %12.6f %12.6f %12.6f %12.6f\n",
                    ega_ext_com[0], ega_ext_com[1], ega_ext_com[2], ega_ext_com[3],
                    lvd_t_pos_est[0], lvd_t_pos_est[1], lvd_t_pos_est[2], lvd_t_pos_est[3]);
            } else {
                fprintf(f_ega, "INPUTS: Est. Com: %12.6f %12.6f %12.6f %12.6f\n",
                    ega_ext_com[0], ega_ext_com[1], ega_ext_com[2], ega_ext_com[3],
                    lvd_t_pos_est[0], lvd_t_pos_est[1], lvd_t_pos_est[2], lvd_t_pos_est[3]);
            }
        }
        if (diag_level == 3) {
            if (f_ega == (FILE *) NULL) {
                printf("\n Internals: curr ext: %12.6f %12.6f %12.6f %12.6f\n",
                    ega_curr_ext[0], ega_curr_ext[1], ega_curr_ext[2], ega_curr_ext[3],
                    ega_onoff_a, ega_onoff_b);
            } else {
                fprintf(f_ega, "\n Internals: curr ext: %12.6f %12.6f %12.6f %12.6f\n",
                    ega_curr_ext[0], ega_curr_ext[1], ega_curr_ext[2], ega_curr_ext[3],
                    ega_onoff_a, ega_onoff_b);
            }
        }
        if (f_ega == (FILE *) NULL) {
            printf("End of Cycle. bb_timetag = %f\n\n", bb_timetag);
        } else {
            fprintf(f_ega, "End of Cycle. bb_timetag = %f\n\n", bb_time
                tag);
        }
    }
}

```

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ega_model.c

```

};
if (diag_time . . 0 && model == 3) {
    diag_flag = 1;
    if (f_ega != (FILE *) NULL) {
        if (fclose(f_ega) != 0) !
            printf ( "Error closing Engine Gimbal Debug File \n" );
    };
};
if (diag_time < 0 && model == 3)
    diag_time = 0;

void?
ega_kinematics (me1_u_vec, me2_u_vec )
{
    d_real      me1_u_vec, me2_u_vec;

    /**
     * local:
     *
     * extc (2)          "calculated" normalized extensions
     * ext_err (2)       normalized extension error
     * angle_step (2)    newton step
     * big_g (2,2)       matrices of partials
     * angle (2)         gimbal angles
     * rate (2)          output gimbal rates (rad/s)
     * accel (2)         output gimbal accels (rad/ s/s)
     * ext (2)           normalized extensions
     * ext_dot (2)       normalized extension rates
     * ext_dot_dot (2)   normalized extension accels
     * mtemp (2,3)       temporary matrix
     * linmap (2,2) and vtemp (2) temporary vectors
     * i, j, k           misc counters
     * convergence       convergence flag
     * counter           counter for newton iterations
     * c1, c2, s1, c2    trig functions
     * td1d2             trans matrix
     * geom              thrust unit vector in engine coords
     * me_str            temp transformation matrix
     */

    d_real      extc[2], ext_err[2], angle_step[2], angle[2], ext[2], ext_err_norm,
                c1, c2, s1, s2, geom[3];

    d_real      big_g[2][2], mtemp[2][3], linmap[2][2], td1d2[3][3], me_str[3][3];

};

int      rea, i, j, convergence, counter;

/ \ REA loop - thrust vector for each REA */
for (rea = 0; rea < 2; rea++) {
    r * decompose extension data and normalize */
    for (i = 0; i < 2; i++) {
        #if 0
            ext[i] = ega_curr_ext[rea * 2 + i] / ega_null_length;
        #endif
        ext[i] = ega_curr_ext [ i * 2 . rea] / ega_null_length;

        /* initialize guess from inverting linear map */
        for (i = 0; i < 2; i++) {
            cross(mtemp[i], u_joint[rea][i], p_joint[rea][i]);

```

```

for (i = 0; i < 2; i++) {
    for (j = 0; j < 2; j++) {
        linmap[i][j] = mtemp[i][j];
    }
}

l2solve(linmap, ext, angle);

/* newton loop */
convergence = 0;
counter = 0;
while (convergence == 0) {
    if (counter > ega_counter_max) {
        /**
         *
         * convergence = 1;
         */
        /* calculate extension and matrix of partials */
        ega_extension (angle, extc, big_g, rea);

        /* evaluate extension error */
        for (i = 0; i < 2; i++) {
            ext_err[i] = ext[i] - extc[i];
        }

        ext_err_norm = sqrt(pow(ext_err[0], 2) +
                               pow(ext_err[1], 2));

        /* test convergence */
        if (ext_err_norm . ega_err_tol)
            convergence = 1;
    }
    if (convergence == 0) !
        /* solve for newton step */
        l2solve(big_g, ext_err, angle_step);

        /* take newton step */
        for (i = 0; i < 2; i++) {
            angle[i] = angle[i] + angle_step[i];
        }

        counter = counter + 1;
    }
}

/* end of newton loop */

if (model == 3 && diag_time > 0 && diag_level == 3 && diag_flag == 0)
{
    if ((f_ega = fopen("/sim/tmp/ega_diags", "w")) == (FILE *) NULL) {
        printf("File Open Failure for EGA diagnostics\n");
    };
    diag_flag = 1;
    if (f_ega == (FILE *) NULL) {
        printf("REA: %3d Angle0: %12.6f Angle1: %12.6f\n", rea, angle[0], angle[1]);
    } else {
        fprintf(f_ega, "REA: %3d Angle0: %12.6f Angle1: %12.6f\n", rea, angle[0], angle[1]);
    };
};
}

```


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ega_model.c

```
/*compute ME thrust unit vector given solution for angles */
/* first compute the null_to_rotated transform */
s1 = sin(angle[0]);
c1 = cos(angle[0]);
s2 = sin(angle[1]);
c2 = cos(angle[1]);
tdld2[0][0] = c2;
tdld2[0][1] = s1 * s2;
tdld2[0][2] = -c1 * s2;
tdld2[1][0] = 0.0;
tdld2[1][1] = c1;
tdld2[1][2] = s1;
tdld2[2][0] = s2;
tdld2[2][1] = -s1 * c2;
tdld2[2][2] = c1 * c2;

geom[0] = 0.0;
geom[1] = 0.0;
geom[2] = -1.0;

/* compute u3 vector in spacecraft coordinates */
if (rea == 0) {
    times_33mat33mattran(me_str, me1_null_trans, tdld2);
    times_33mat3vec(me1_u_vec, me_str, geom);
} else {
    times_33mat33mattran(me_str, me2_null_trans, tdld2);
    times_33mat3vec(me2_u_vec, me_str, geom);
}

/* end of rea loop */

void
ega_extension(angle, ext, big_g, rea)
    d_real *angle, *ext;
    d_real big_g[2][2];
    int rea;

/*
 * In:    angle[2]:    engine gimbal angles (rad)
 *
 * Out:   ext[2]:      normalized ega extensions big_g[2][2]:    partial
 * derivative matrix rea:    number of the engine assembly under
 * consideration
 */

{
    /**
     * local:
     *
     * s1          sin of angle(1) c1          cos
     * of angle(1) s2          sin of angle(2) c2 os of
     * angle(2)
     *
     * alpha(2)    intermediate    9(2,2)          alpha
     * derivatives h(2, 2,2)    second alpha derivatives
     *
     * stempl->2    temporary scal ars vtempl (3) ary vector
     * mtempl->4 (3,3)    temporary matrices pmj (2,3) _joint t -
     * u_joint gamma (3,3)    identity minus rotation matrix
     * gammat (3,3)    gamma transpose dgamma (2 , 3,3 ) erivative of
     * gamma dgamm (2,3,3)    dgamma transpose i, j , k
     * isc counters
     */
}
```

```
d_real    s1, c1, s2, c2, alpha[2], stempl, stempl2, vtempl[3];

int        i, j;

d_real    gamma_local[3][3], gammat[3][3], g[2][2], mtempl[3][3], mtem
p2[3][3],
           mtemp[3][3], pmj[2][3], dgamma[2][3][3], dgamm[2][3][3];

s1 = sin(angle[0]);    /* trig functions */
c1 = cos(angle[0]);
s2 = sin(angle[1]);
c2 = cos(angle[1]);

gamma_local[0][0] = 1. - c2;    /* form gamma and its derivatives */
gamma_local[0][1] = -s1 * s2;
gamma_local[0][2] = c1 * s2;
gamma_local[1][0] = 0.;
gamma_local[1][1] = 1. - c1;
gamma_local[1][2] = -s1;
gamma_local[2][0] = -s2;
gamma_local[2][1] = s1 * c2;
gamma_local[2][2] = 1. - c1 * c2;

dgamma[0][0][0] = 0.;
dgamma[0][0][1] = -c1 * s2;
dgamma[0][0][2] = -s1 * s2;
dgamma[0][1][0] = 0.;
dgamma[0][1][1] = s1;
dgamma[0][1][2] = -c1;
dgamma[0][2][0] = 0.;
dgamma[0][2][1] = c1 * c2;
dgamma[0][2][2] = s1 * c2;

dgamma[1][0][0] = s2;
dgamma[1][0][1] = -s1 * c2;
dgamma[1][0][2] = c1 * c2;
dgamma[1][1][0] = 0.;
dgamma[1][1][1] = 0.;
dgamma[1][1][2] = 0.;
dgamma[1][2][0] = -c2;
dgamma[1][2][1] = -s1 * s2;
dgamma[1][2][2] = c1 * s2;

/* calculate the alpha's */
transpose_33mat(gammat, gamma_local);
for (i = 0; i < 2; i++) {
    times_33mat3vec(vtempl, gammat, p_joint[rea][i]);
    minus_3vec(pmj[i], p_joint[rea][i], u_joint[rea][i]);
    stempl = dot3(vtempl, pmj[i]);
    stempl2 = dot3(vtempl, vtempl);
    alpha[i] = -stempl + 0.5 * stempl2;
}

/* extensions */
for (i = 0; i < 2; i++) {
    ext[i] = sqrt(1. + 2. * alpha[i]) - 1.;
}

/* calculate derivative matrices */

/* get g */
for (i = 0; i < 2; i++) {
    transpose_33mat(dgamm[i], dgamma[i]),
}
```

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ega_model.c

```
}
for (i = 0; i < 2; i++) {
    for (j = 0; j < 2; j++) {
        times_33mat3vec(vtemp1, dgammat[i], p_joint[real[i]);
        stemp1 = dot3(vtemp1, pm[j]);
        times_33mat33mat(mtemp1, dgammat[j], gammat ,
        transpose_33mat(mtemp2, mtemp1);
        plus_spmat(&mtemp3[0][0], &mtemp1[0][0],
        &mtemp2[0][0], 3);
        times_33mat3vec(vtemp1, mtemp3, p_joint[real[i] ,
        stemp2 = dot3(vtemp1, p_joint[real[i]);
        g[i][j] = -stemp1 + 0.5 * stemp2;
    }
}

/* get big_g */
for (i = 0; i < 2; i++) {
    for (j = 0; j < 2; j++) {
        big_g[i][j] = g[i][j] - 1 + ext[i]
    }
}

/* end of ega_extension */

void
l2solve(a, b, angle)
/*
 * solves 2x2 ax = b input = [ a[1][2] b[2] output angle[2]
 */
{
    d_real *b, *angle;
    d_real a[2][2];

    d_real det;

    det = a[0][0] * a[1][1] - a[1][0] * a[0][1];

    if (det == 0.) {
        printf("aaaaack! ega model: 2x2 map singular");

        angle[0] = (a[1][1] * b[0] - a[0][1] * b[1]) / det;
        angle[1] = (-a[1][0] * b[0] + a[0][0] * b[1]) / det;
    }
}
```

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gyro_model.c

```
/* gyro_model.c */
/* cassini itl gyro model */

/* for the d_real typedef */
#include "types-darts.h"

/* for matrix subroutines */
#include "linalg-darts.h"

/* standard */
#include <math.h>
#include <string.h>

/* Diagnostics */
extern int model;
extern int diag_time;
extern int diag_level;
extern FILE *f_gyro;
extern int diag_flag;
extern d_real bb_timestep;

/* local */
#include "gyro_model.h"

/* namelist data */
d_real gyro_sens_a1[3], gyro_sens_a2[3], gyro_sens_a3[3], gyro_sens_a4[3],
      gyro_sens_b1[3], gyro_sens_b2[3], gyro_sens_b3[3], gyro_sens_b4[3],
      gyro_rate_quant;

/* local */
int gyro_onoff_a, gyro_onoff_b;
d_real quant_remainder[8];

/** Modification 29 July 96 J. Bunn:
    Changed onoff_a(b) to gyro_onoff_a(b) to avoid model conflicts
    **/

void gyro_init()
{
    int i;

    /* namelist parameters */
    gyro_rate_quant = 0.5e-6;

    /*
     * Define gyro sense axes, Ref: IOM 3413-94-010, IRU Location and
     * Orientation: Gyro Input Axis Orientation Doug Bernard July 28 1994
     */
    gyro_sens_a1[0] = 0.418432;
    gyro_sens_a1[1] = -0.908248;
    gyro_sens_a1[2] = 0.;

    gyro_sens_a2[0] = -0.642229;
    gyro_sens_a2[1] = -0.295876;
    gyro_sens_a2[2] = -0.707107;

    gyro_sens_a3[0] = -0.642229;
    gyro_sens_a3[1] = -0.295876;
    gyro_sens_a3[2] = 0.707107;

    gyro_sens_a[0] = 0.5;
    gyro_sens_a[1] = 0.866025;

    /* for testing gyro_sens_a1[0] = 1.; gyro_sens_a1[1] = 0.;
     * gyro_sens_a1[2] = 0.; gyro_sens_a2[0] = 0.; gyro_sens_a2[1] =
     * 1.; gyro_sens_a2[2] = 0.; gyro_sens_a3[0] = 0.; gyro_sens_a3[1] =
     * = 0.; gyro_sens_a3[2] = 1.;
     */

    gyro_sens_b1[0] = 0.995182;
    gyro_sens_b1[1] = -0.0917517
    gyro_sens_b1[2] = 0.

    gyro_sens_b2[0] = -0.0648783
    gyro_sens_b2[1] = -0.704124;
    gyro_sens_b2[2] = -0.707107.

    gyro_sens_b3[0] = -0.0648783;
    gyro_sens_b3[1] = -0.704124;
    gyro_sens_b3[2] = 0.707107;

    gyro_sens_b4[0] = -0.5;
    gyro_sens_b4[1] = 0.866025;
    gyro_sens_b4[2] = 0.;

    /* for testing gyro_sens_b1[0] = 1.; gyro_sens_b1[1] = 0.;
     * gyro_sens_b1[2] = 0.; gyro_sens_b2[0] = 0.; gyro_sens_b2[1] =
     * 1.; gyro_sens_b2[2] = 0.; gyro_sens_b3[0] = 0.; gyro_sens_b3[1] =
     * = 0.; gyro_sens_b3[2] = 1.;
     */

    /* init */
    for (i = 0; i < 8; i++)
        quant_remainder[i] = 0.

    /* default gyro a on and gyro b off */
    gyro_onoff_a = 1;
    gyro_onoff_b = 1;
}

void gyro_onoff(onoff_str,
               char onoff_str[])
{
    if (!strcmp(onoff_str, "irua on")
        gyro_onoff_a = 1;
    if (!strcmp(onoff_str, "irua off")
        gyro_onoff_a = 0;
    if (!strcmp(onoff_str, "irub on")
        gyro_onoff_b = 1;
    if (!strcmp(onoff_str, "irub off")
        gyro_onoff_b = 0;

    gyro_model(rate, gyro_bias)
    d_real rate;
    int gyro_bias[]

    int i;
    d_real sens_rate[8];
    d_real gyro_bias_real gyro_bias_whole;

    /* compute rates along gyro sense axes */
}
```

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gyro_model.c

```
sens_rate[0] = dot3(rate, gyro_sens_a1);
sens_rate[1] = dot3(rate, gyro_sens_a2);
sens_rate[2] = dot3(rate, gyro_sens_a3);
sens_rate[3] = dot3(rate, gyro_sens_a4);
sens_rate[4] = dot3(rate, gyro_sens_b1);
sens_rate[5] = dot3(rate, gyro_sens_b2);
sens_rate[6] = dot3(rate, gyro_sens_b3);
sens_rate[7] = dot3(rate, gyro_sens_b4);

/* Loss Less quant */
for (i = 0; i < 9; i++) {
    gyro_bias_real = sens_rate[i] / gyro_rate_quant
        + quant_remainder[i];
    quant_remainder[i] = modf(gyro_bias_real, &gyro_bias_whole);
    gyro_bias[i] = (int) gyro_bias_whole;
}

/* overwrite with zeros if off */
if ('gyro_onoff_a')
    for (i = 0; i < 4; i++)
        gyro_bias[i] = 0;
if ('gyro_onoff_b')
    for (i = 4; i < 8; i++)
        gyro_bias[i] = 0;

/* Diagnostics */
if (model == 4 && diag_time -- > 0) {
    if (diag_flag == 0) {
        if ((f_gyro = fopen("/sim/tmp/gyro_diags", "w")) == (FILE *) NULL) {
            printf("File Open Failure for GYRO Diagnostics\n");
            diag_flag = 1;
        }

        if (diag_level == 1 || diag_level == 2 || diag_level == 3) {
            if (f_gyro == (FILE *) NULL) {
                printf("GyroBiases:\n");
                for (i = 0; i < 8; i++) {
                    printf("%12.6d\n", gyro_bias[i]);
                }
                printf("\n");
            } else {
                fprintf(f_gyro, "GyroBiases:\n");
                for (i = 0; i < 8; i++) {
                    fprintf(f_gyro, "%12.6d\n", gyro_bias[i]);
                }
                printf(f_gyro, "\n");
            }
        }

        if (diag_level == 2 || diag_level == 3) {
            if (f_gyro == (FILE *) NULL) {
                printf("Rates: %12.6f %12.6f %12.6f\n\n", rate[0], rate[1], rate[2]);
            } else {
                fprintf(f_gyro, "Rates: %12.6f %12.6f %12.6f\n\n", rate[0], rate[1], rate[2]);
            }
        }

        if (diag_level == 3) {
            if (f_gyro == (FILE *) NULL) {
                for (i = 0; i < 8; i++) {
                    printf("sens_rate %12.6f quant_remainder %12.6f\n", sens_rate[i], quant_remainder[i]);
                }
            } else {
                fprintf(f_gyro, "sens_rate %12.6f quant_remainder %12.6f\n\n", sens_rate[i], quant_remainder[i]);
            }
        }
    }
}

if (diag_time == 0 && model == 4) {
    diag_flag = 0;
    if (f_gyro == (FILE *) NULL) {
        if (fclose(f_gyro) != 0) {
            printf("Error closing Gyroscope Diagnostic File!\n");
        }
    }
}

if (diag_time < 0 && model == 4) {
    diag_time = 0;
}
```

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RW.C

```

/*****
 * r_wheel *
 * ****
 */

/* DESCRIPTION
$id: rw.c,v 1.27 1997/ 01/2723:02:53its1Exp$
Thisfile contains the simulation for the CASSINI reaction wheels for use
in the Integration and Test Laboratory.
*/

/** REVISION HISTORY:
23 June 95: Jason Bunn Creation
23 June - 5 July: Jason Bunn Initial Development
10 July: Jason Bunn Added Power Model and Integration Coefficients
14 July: Jason Bunn Began adding interface modules
21 July: Jason Bunn delivered code to J. Roberts for integration
7 August: Recent Updates :
    'Tachometer Model Corrected
    Bugs fixed to facilitate Integration
    Expanded to four reaction wheels
27 August 96: Changed to new power model
    changed tachometer function declaration to short
    Changed derivation of scale factor from .1755/128 to .1755 /127
30 August 96: Coded switch from copies to arrays
20 September 96: Added code to simulate RTIOU reset
24 September 96: Added Dahl state friction limiter and changed scale factor
    to reflect latest change as per FSC #423, FSW A5.1.0
15 October 96: Implemented separate current scale factors per FSC #450, FSW A5.2.0
**/

/** INPUTS FOR EACH WHEEL:
Information from the registers concerning the commanded torque.
**/

/** OUTPUTS FOR EACH WHEEL:
Current state of the reaction wheel, including current, tach
output and read back commanded torque.
**/

/* OPERATION:
At the start of a loop, the simulation checks to see if power is on. If, so
the commanded torque is read and added to the state. If not, the commanded
torque register is not read. When power is first supplied, the registers are
cleared to zero. The state is then propagated in time, followed
by an output state where the current state variables of interest are passed
to the registers. The register file communicates with the RTIOU and passes
the data to the AACS bus through the RTIOU when necessary. Loops occur
every 62.5 ms.
*/

#include <math.h>
#include <stdio.h>
#include "serverDemo.h"
#ifdef SUN
#include "vme_addresses.h"
#include "assembly.h"

extern int peek8 ();
extern int poke8 ();
extern char *assem_rwx1;
extern char *assem_hvx2;
extern char *assem_rwx3;
extern char *assem_rwx4;

```

```

extern struct assem_board card[6];

#endif
void RWX_power_on ();

/** STRUCTURE definitions **/

/* RTIOU Registers */
struct RWA_reg {
    int power;
    char reg01wr; /* dummy write to enable torw CMD */
    char reg04wr; /* load mux control reg */
    char reg06wr; /* Torque CMD */
    char reg02rd; /* Dummy read to load tach reg */
    char reg03rd; /* Upper byte of tach reg */
    char reg04rd; /* Lower byte of tach reg */
    char reg05rd; /* A/D Converter */
    char reg06rd; /* Torque CMD wrap-around */
    char reg07rd; /* Time out Test */
};

struct RWAParams {
    double cog_amp;
    double cog_phi;
    double dahl_amp;
    double dahl_ang;
    double dyn_amp;
    double dyn_phi;
    double int_stp_size;
    double max_mtr_torg;
    double phases;
    double poles;
    double rate_cutoff;
    double rate_cuton;
    double rip_amp;
    double rip_phi;
    double slots;
    double stat_amp;
    double stat_phi;
    double tq_wrd_bts;
    double tach_magnets;
    double tach_pos_quant;
    double vlsr_amp;
    double wheel_inertia;
    double current_scale_factor;
    /**
cog_amp -Description: Reluctance cogging torque amplitude
Units: Nm
cog_phi -Description: Reluctance cogging torque phase
Units: rad
dahl_amp -Description: Coulomb level for Dahl model of bearing
drag torque
Units: Nm
dahl_ang -Description: Amplitude of bearing rotation required for t
he
9% Dahl model of bearing drag torque to reach 9
of its final value (Coulomb level)
dyn_amp -Description: Amplitude for dynamic torques due to wheel
products of inertia
Units: Nm/(rad/sec)^2
dyn_phi -Description: Phase angle for dynamic torques due to wheel
products of inertia
Units: rad

```

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```
int_stp_size -Description: Numerical integration step size
Units: sec
max_mtr_t_orq -Description: Motor torque limit
Units: Nm
phases -Description: Number of motor phases
Units: None
poles -Description: Number of motor poles (2*#poles pairs)
Units: None
rate_cut off -Description: RWA rate at which the motor disables motor
torque. A safety feature to prevent RWA damage
due to overspeed.
Units: rad/sec
rate_cut On -Description: RWA rate at which the motor re-enables motor
torque once it has been shutdown due to an
overspeed condition.
Units: rad/sec
rip_amp -Description: Commutation ripple torque phase
Units: rad
slots -Description: Number of motor winding slots
Units: None
stat_amp -Description: Amplitude for static forces due to wheel
center of mass offset from spin axis
Units: N/(rad/sec)^2
stat_phi -Description: Phase angle for static forces due to wheel
center of mass offset from spin axis
Units: rad
tach_magnets -Description: The number of magnets in the tachometer. (At least 2
are required) A double variable. Unitless
tq_wrd_bts -Description: Motor torque word length
Units: bits
visc_amp -Description: Viscous friction torque for bearing
Units: Nm/(rad/sec)
...

/* derived */
double cog_freq;
double dahl_sig;
double rip_freq;
double torq_const;
double w_cog_cutoff;
double w_rip_cutoff;
double w_sd_cutoff;

/**
cog_freq -Description: Reluctance cogging torque" frequency"
Unit: cycles/rad
dahl_sig -Description: Dahl rest slope (change in friction torque
per change in bearing angle at torque=0
point) for Dahl model of bearing drag torque
Units: Nm/rad
rip_freq -Description: Commutation ripple torque "frequency"
Units: cycles/rad
torq_const -Description: Motor torque resolution
Units: Nm per bit
w_cog_cutoff -Description: Angular rate at which the reluctance cogging
torque frequency reaches the Nyquist sampling
frequency. At this point, cogging torques
would be aliased in the simulation, so they
are set to zero
Units: rad/sec
w_rip_cutoff -Description: Angular rate at which the commutation ripple
torque frequency reaches the Nyquist sampling
frequency. At this point, cogging torques
would be aliased in the simulation, so they
```

```
are set to zero.
Units: rad/sec
w_sd_cutoff -Description: Angular rate at which the commutation ripple
torque frequency reaches the Nyquist samplin
frequency. At this point, cogging torques
would be aliased in the simulation, so they
are set to zero
Units: rad/sec

9
**i
};

/* State Vector and State Derivative */
struct wheel_state {
double position; /* Position of Wheel */
double rate; /* Angular Velocity of Wheel */
double dahl; /* dahl friction term */
};

struct wheel_deriv {
double posd; /* Position Derivative (Angular Velocity) */
double rated; /* Angular Velocity Deriv. (Angular
Acceleration) */
double dahld; /* Dahl friction term rate of change */
};

struct RWAParams rwa_model[4];

struct RWA_reg rwa_reg[4];

struct wheel_state state[4];

struct wheel_state temp_state_1[4];

struct wheel_state temp_state_2[4];

struct wheel_state temp_state_3[4];

struct wheel_deriv stated1[4];
struct wheel_deriv stated2[4];
struct wheel_deriv stated3[4];
struct wheel_deriv stated4[4];

/** Global Variables */
double dt = 0.0625;

double coef_1 = 0.5;
double coef_2 = 0.5;
double coef_3 = 1;
double coef_4 = 0.166667;
double coef_5 = 0.333333;
double coef_6 = 0.233333;
double coef_7 = 0.166667;

double fractional_prev_tach[4];
```

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```
double      overspeed[4];
double      nxt_overspeed[47];
double      power[4];
double      torq_wrd[4];
double      torque[4];
short       tach[4];
short       old_tach_output[4];
short       tach_output[4];
int         rw_init[4];
char        *assem_rwx[4];

int         rwa_flag[4] = {0, 0, 0, 0};
```

```
/* FUNCTIONS */
#define SUN
char
peek8(char 'x')

return 'x';
```

```
char
poke8(char 'x', char c)

*x = c;
return c;
```

```
#endif

/* dsign */
double
dsign(
    double a,
    double b)

    if (b >= 0)
        return fabs((float) a) ;
    return -fabs((float) a) ;
;
```

```
/* Initial Parameters */
void
RWA_load_def(rwp, i)
    struct RWAParam_s *rwp;
    int i;

{
    FILE *fp;
    char *a;
    if (i == 0)
        a = "/sim/dynamics/rw_params_1";
    if (i == 1)
        a = "/sim/dynamics/rw_params_2";
    if (i == 2)
        a = "/sim/dynamics/rw_params_3";
    if (i == 3)
        a = "/sim/dynamics/rw_params_4";

    if ((fp = fopen(a, "r")) != NULL) {
        fscanf(fp, "%lf", &rwp->cog_amp);
        fscanf(fp, "%lf", &rwp->cog_phi);
        fscanf(fp, "%lf", &rwp->dahl1_amp);
        fscanf(fp, "%lf", &rwp->dahl1_ang);
    }
```

```
fscanf(fp, "%lf", &rwp->dyn_amp);
fscanf(fp, "%lf", &rwp->dyn_phi);
fscanf(fp, "%lf", &rwp->int_tstp_size);
fscanf(fp, "%lf", &rwp->max_mtr_to_rq);
fscanf(fp, "%lf", &rwp->phases);
fscanf(fp, "%lf", &rwp->poles);
fscanf(fp, "%lf", &rwp->rate_cutoff);
fscanf(fp, "%lf", &rwp->rate_cut_on);
fscanf(fp, "%lf", &rwp->rip_amp);
fscanf(fp, "%lf", &rwp->rip_phi);
fscanf(fp, "%lf", &rwp->slots);
fscanf(fp, "%lf", &rwp->stat_amp);
fscanf(fp, "%lf", &rwp->stat_phi);
fscanf(fp, "%d", &rwp->tq_wrd_bts);
fscanf(fp, "%lf", &rwp->visc_amp);
fscanf(fp, "%d", &rwp->tach_magnets);
fscanf(fp, "%lf", &rwp->wheel_inertia);
fscanf(fp, "%lf", &rwp->current_scale_factor);
fclose(fp);
```

```
};
```

```
};
```

```
void
RWX_power_off ( struct RWA_reg *rwp, char *assem_base )
```

```
/* Set commanded torque to zero and power to off. */
rwp->reg06wr = 0;
rwp->power = 0;
/* Clear RAM so that power on functions smoothly */
poke8(assem_base + 2 * 1 + 1, 0);
poke8(assem_base + 2 * 2 + 1, 0);
poke8(assem_base + 2 * 3 + 1, 0);
poke8(assem_base + 2 * 4 + 1, 0);
poke8(assem_base + 2 * 5 + 1, 0);
poke8(assem_base + 2 * 6 + 1, 0);
poke8(assem_base + 2 * 7 + 1, 0);
```

```
..
```

```
/* Read information from registers */
void
RWX_getbyte(struct RWA_reg * rwp, char *assem_base, short *tach)
```

```
int x;
/**
    x = peek8 (assem_base + 2 * Poweronregister + 1);
*/
x = read_rwa_power (assem_base);
if (x == 1) { /* Is power on? */
    if (rwp->power == 0) { /* If power is on, is it a POR? */
        RWX_power_on (rwp, Lath);
    };
    /* get Torque Enable Command */
    rwp->reg01wr = peek8 (assem_base + 2 * 1 + 1);
    /* get 2's complement Torque Command */
    rwp->reg06wr = peek8 (assem_base + 2 * 5 + 1);
} else {
    RWX_power_off (rwp, assem_base);
};
```

```
};
```

```
/* Write information to registers */
void
RWX_putbyte ( struct RWA_reg *rwp, char *assem_base )
```

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```
/** echo Torque command back to FSW
poke8 (assem_base + 2 * 5 + 1, rwp->reg05rd);
Asem sim card uses a RAM, therefore, we do not want to overwrite new
torque information. **/
```

```
/* A/D Converter info */
poke8 (assem_base + 2 * 5 + 1, rwp->reg05rd);
```

```
/* Upper Byte of Tachometer Output */
poke8 (assem_base + 2 * 3 + 1, rwp->reg03rd);
```

```
/* Lower Byte of Tachometer Output */
poke8 (assem_base + 2 * 4 + 1, rwp->reg04rd);
```

```
/* Dummy read to load tach register */
poke8 (assem_base + 2 * 2 + 1, rwp->reg02rd);
```

```
/* Time out Test */
poke8 (assem_base + 2 * 7 + 1, rwp->reg07rd);
```

```
};
```

```
1' Dahl Friction */
/* Adopted from Matt Wette's Code */
/*
* This routine models the analog portion of the Cassini Reaction Wheel
* Assembly (RWA) Dahl friction model.
*
* The routine accepts the current value of the RWA bearing angle, bearing
* velocity, and the current value of the Dahl model bearing and friction
* torque. It then returns the time derivative of the Dahl model bearing
* friction torque.
*/
```

```
double
RWA_dahl ( struct RWAParam_s rwp,
           struct wheel_state * state, // gimbal angle from dyn (rad) */
           /* angle rate from dyn (rad/sec) */
           /* Dahl fric from dahl-model (Nm) */
           double fric_dot)
{
    /* time deriv of dahl fric (Nm/s) */
    double dahl_fric_lim;
    double dtorq_dangle;
    double temp;

    /* Compute the time derivative of the Dahl bearing torque: */
    if (fabs(state->dahl) >= (rwp->dahl_amp)) {
        dahl_fric_lim = dsign((rwp->dahl_amp), state->dahl);
    } else {
        dahl_fric_lim = state->dahl;
    }

    temp = 1.0 + dsign(1.0, state->rate) * dahl_fric_lim / (rwp->dahl_amp);
    dtorq_dangle = -(rwp->dahl_sig) * dsign(1.0, temp) * fabs(temp);
    (fric_dot) = state->rate, dtorq_dangle;
    return (fric_dot);
};
```

```
/* Power Model Current = Power I 30 Volts */
void
rwa_pwr (
    double rw_rate,
    double mtr_tq,
```

```
double *pto Eal)
```

```
/**
@doc@ @name rwa_pwr
@doc@ @disc This subroutine calculates the power usage for a single reaction
@doc@ @disc wheel based on wheel speed and applied torque values
@doc@ @returns Ptotal
@doc@ @req model the analog portion of the reaction wheel
*/
```

```
/**
* Inputs : rw_rate - wheel rate (rad/sec) mtr_tq - torque from motor (Nm)
*
* Outputs: Ptotal - Total power usage (Watt s)
*/
```

```
/* Based on Appenix to CAB dated 11-94 changed on 5-24-96 by L.Montanez */
```

```
/** New model based on Model Validation Team input 8/9/96
* Changed 9/27/96 by J. Bunn
*/
```

```
double c0Power, c1Power, c2Power, c3Power, c4Power;
c0Power = 9.4999355; /* Watts */
c1Power = 60.4512337; /* Watts/ (N-m) * I
c2Power = 1.0354894; /* Watts/ (N-m) per rad/sec * I
c3Power = 0.0028060; /* Watts/ (rad/sec) */
c4Power = 4.00; /* Watts */
```

```
if (mtr_tq < 0.0)
    *ptotal = (c0Power + (c1Power * fabs(mtr_tq)) -
               (c3Power + c2Power * fabs(mtr_tq)) * rw_rate);
else
    *ptotal = (c0Power + (c1Power * mtr_tq) +
               (c3Power + c2Power * mtr_tq) * rw_rate);
if (*ptotal < 0.0)
    *ptotal = c4Power;
else
    *ptotal += c4Power;
```

```
};
```

```
void
RWA_ana(
    struct RWAParam_s rwp,
    double torq_word,
    struct wheel_state * state,
    double *ovr_spd_flg,
    double *torq,
    double *power,
    double *nxt_o_s_f)

/**
@doc@ @name RWA_ana
@doc@ @disc This routine accepts the current value of the RWA torque cmd,
@doc@ @disc bearing angle, bearing velocity, and the current value of the
@doc@ @disc Dahl model bearing friction torque and overspeed flag
@doc@ @returns torq, stat_forcel, stat_force2, dyn_torque1, dyn_torque2, power
@doc@ @returns nxt_o_s_f
@doc@ @functions called fabs, rwa_pwr
@doc@ @req model the analog portion of the reaction wheel
*/
```

```
double cogging_torq;
```


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```
double motor_torque;
double ripple_torque;
double visc_fric;
double x;
/*
 * Check for an RWA overspeed condition and compute the next value of
 * the overspeed indicator flag. A non-zero value for the flag
 * indicates an overspeed condition.
 */
if (ovr_spd_flg == 0.0) {
    if (fabs(state->rate) >= (rwp->rate_cutoff)) {
        *next_o_s_f = 1.0;
    }
    else {
        *next_o_s_f = 0.0;
    }
}
else {
    if (fabs(state->rate) <= (rwp->rate_cutoff)) {
        *next_o_s_f = 0.0;
    }
    else {
        *next_o_s_f = 1.0;
    }
}
*ovr_spd_flg = *next_o_s_f;

/* Compute motor torque if an overspeed condition exists, null the
 * motor torque:
 */
if (*ovr_spd_flg == 0.0) {
    motor_torque = ovr_word * rwp->torq_const;
}
else {
    motor_torque = 0.0;
}

/* Compute commutation ripple torque: */
if (fabs(state->rate) >= (rwp->w_rip_cutoff)) {
    ripple_torque = 0.0;
}
else {
    x = (rwp->rip_freq) * state->position + (rwp->rip_phi);
    ripple_torque = (rwp->rip_amp) * motor_torque * sin(x);
}

/* Compute viscous friction torque: */
visc_fric = -(rwp->visc_amp) * state->rate;

/* Compute the total torque that will be applied along the RWA gimbal
 * in the dynamics simulation:
 */
*torq = motor_torque + ripple_torque + state->dahl + visc_fric;

/* Compute the power used by the RWA: */
rwa_pwr(state->rate, motor_torque, power);
};

/* Calculate State Derivative */
void
rwa_deriv(
    struct wheel_state * state,
    double torq_word,
    struct wheel_deriv * stated,
    double *over_speed,
```

```
double *nxt_overspeed,
struct RWAParam_s * params
double *torque,
double *power)
{
    RWA_ana(params, torq_word, state, over_speed, torque, power, nxt_overspeed);

    stated->posd = state->rate;
    stated->rated = *torque / params->wheel_inertia;
    stated->dahld = RWA_dahl(params, state, stated->dahld);

    /* Load Initial Values */
    void
    RWA_load_def(
        struct RWA_reg * rwp,
        short *tach_reg)
    {
        rwp->power = 0;
        rwp->reg05wr = 0;
        rwp->reg02rd = 0;
        rwp->reg03rd = 0;
        rwp->reg04rd = 0;
        rwp->reg05rd = 0;
        rwp->reg06rd = 0;
        *tach_reg = 0;
    }

    /* Power On Procedures */
    void
    RWA_power_on(
        struct RWA_reg rwp, short *tach)
    {
        rwp->power = 1;
        rwp->reg02rd = 0;
        rwp->reg03rd = 0;
        rwp->reg04rd = 0;
        rwp->reg05rd = 0;
        rwp->reg06rd = 0;
        *tach = 0;
    }

    /* Initialization Routine */
    void
    RWA_upd_params(struct RWAParam_s * rwp)
    {
        rwp->cog_freq = (rwp->slots);
        rwp->dahl_sig = 4.0 * (rwp->dahl_amp) / (rwp->dahl_ano);
        rwp->rip_freq = (rwp->phases) * (rwp->poles);
        rwp->torq_const = (rwp->max_mtr_torq) /
            ((1 << (rwp->stq_wrd_bts - 1)) - 1);
        rwp->w_cog_cutoff = 3.14159 / ((rwp->cog_freq)
            * (rwp->int_stp_size));
        rwp->w_rip_cutoff = 3.14159 / ((rwp->rip_freq)
            * (rwp->int_stp_size));
        rwp->w_sd_cutoff = 3.14159 / (rwp->int_stp_size);
        rwp->tach_pos_quant = 2.0 * 3.14159265358979 / rwp->tach_magnets;
    }

    /* Initialize State and State Derivative Structures */
    void
    state_init(struct wheel_state * state)
    {
        state->position = 0.0;
        state->rate = 0.0;
    }
}
```

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```
state->dahl = 0 0;

void
stated_init(struct wheel_deriv *stated)
{
    stated->posd = 0 0;
    stated->rate = 0 0;
    stated->dahld = 0 0;
}

#ifdef OLD
double
tachometer(struct RWAParam_s *rwa_model, struct wheel_state *state, short *old_tach_output, short *tach_output)
{
    double    tach_quant;
    double    inc_tach_output;

    *old_tach_output = *tach_output;
    tach_quant = 2 0 ' 3 141592654 / rwa_model->tach_magnets;
    inc_tach_output = (state->rate / tach_quant) - *old_tach_output;
    *tach_output = *old_tach_output + inc_tach_output;
    return (inc_tach_output);
};
#endif

short
tachometer(struct RWAParam_s *rwa_model, struct wheel_state *state, double *fractional_prev_tach)
{
    double    real_tach;
    double    ideal_tach;
    double    tach_quant;

    tach_quant = 2 0 ' 3.141592654 / rwa_model->tach_magnets;

    ideal_tach = (state->rate / tach_quant) * .125;
    real_tach = ideal_tach * fractional_prev_tach;
    *fractional_prev_tach = real_tach - (int)real_tach;
    return ((short)real_tach);
}

void
Output(struct RWReg *rwa_reg, struct RWAParam_s *rwa_model, struct wheel_state *state, double *power, short *tach, double *fractional_prev_tach)
{
    short    temp_tach;
    short    overtach;
    short    undertach;
    double    current;

    current = ((*power / 30.0) / (rwa_model->current_scale_factor)) + 128.0;
    rwa_reg->reg05rd = current;
    rwa_reg->reg06rd = rwa_reg->reg06wr;
    tach = tachometer(rwa_model, state, fractional_prev_tach);
    temp_tach = *tach;
    overtach = 0;
    undertach = 0;
    if (*tach > 2047)
        overtach = 0x8000;
    if (*tach < -2048)
        undertach = 0x4000;
    temp_tach = (*tach & 0xFFF) | overtach | undertach;
    rwa_reg->reg03rd = (temp_tach >> 8 & 0xFF);
    rwa_reg->reg04rd = (temp_tach & 0xFF);
}
```

```
rwa_reg->reg02rd = (0xFFFF & 0xFF);
rwa_reg->reg07rd = (0xFF);
};

#ifdef SUN
char    assem_rwx1[0xffff];
char    assem_rwx2[0xffff];
char    assem_rwx3[0xffff];
char    assem_rwx4[0xffff];
#endif

int
read_rwa_power(base)
    char    *base;
{
    int    power, pwr_status;

    pwr_status = peek8(base + (0x8000 + 1));
    power = 0;
    if ((pwr_status & 0x04) == 0x04)
        power = 1;

    return (power);
};

int
rwa_init()
{
    int    i;

    for (i = 0; i < 4; i++) {
        /* Initialize */
        fractional_prev_tach[i] = 0.0;
        overspeed[i] = 0;
        next_overspeed[i] = 0;
        power[i] = 0;
        torque_word[i] = 0;
        torque[i] = 0;
        tach[i] = 0;
        old_tach_output[i] = 0;
        tach_output[i] = 0;
        rw_init[i] = 0;

        /* Reset registers to zero and clear any accumulators */
        RWA_load_def(&rwa_model[i], i);
        RWA_upd_params(&rwa_model[i]);
        RWX_load_def(&rwa_reg[i], &tach[i]);

        /* Initialize state and derivative structures */
        state_init(&state[i]);
        state_init(&temp_state_1[i]);
        state_init(&temp_state_2[i]);
        state_init(&temp_state_3[i]);

        stated_init(&stated1[i]);
        stated_init(&stated2[i]);
        stated_init(&stated3[i]);
        stated_init(&stated4[i]);

        rw_init[i] = 1;
    }

    assem_rwx[0] = assem_rwx1;
}
```

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```
assem_rwx[1] = assem_rwx2;
assem_rwx[2] = assem_rwx3;
assem_rwx[3] = assem_rwx4;
return 0;
};

int
rwa_loop()
{
    int i;
    for (i = 0; i < 4; i++) {
        /* Read Registers */
        RWX_getbyte(&rwa_reg[i], assem_rwx[i], &tach[i]);
        if (rwa_init[i] == 0)
            return 0;

        if ((rwa_reg[i].reg0lwr != 0) && (rwa_flag[i] == 1))
            rwa_flag[i] = 2;
        else if ((rwa_reg[i].reg0lwr != 0) && (rwa_flag[i] == 2))
            rwa_flag[i] = 0;
        else if ((rwa_reg[i].reg0lwr != 0) && (rwa_flag[i] == 0)) {
            poke8(assem_rwx[i] + 2 * 6 + 1, 0);
            rwa_reg[i].reg06wr = 0;
        };
        if (rwa_reg[i].reg0lwr == 0 && rwa_reg[i].power == 1) {
            rwa_flag[i] = 1;
            poke8(assem_rwx[i] + 2 * 1 + 1, 0xFF);
        };

        /* Compute Torque Word */
        if (rwa_reg[i].reg06wr > rwa_model[i].max_mtr_torq / rwa_model[i].torq_c
onst)
            torq_word[i] = dsign(rwa_model[i].max_mtr_torq / rwa_model[i].to
rq_const, rwa_reg[i].reg06wr);
        else
            torq_word[i] = rwa_reg[i].reg06wr;

        /* Propagate State */
        /*
         * 4th order numerical integration. Time step = dt = 0.0625
         * seconds. Calculates the next values of the state variables
         */

        rwa_deriv(&state[i], torq_word[i], &stated1[i], &overspeed[i], &nxt_ove
speed[i],
                &rwa_model[i], &torque[i], &power[i]);
        temp_state_1[i].position = state[i].position + coef_1 * dt * stated1[i]
posd;
        temp_state_1[i].rate = state[i].rate + coef_1 * dt * stated1[i].rated;
        temp_state_1[i].dahl = state[i].dahl + coef_1 * dt * stated1[i].dahld;

        rwa_deriv(&temp_state_1[i], torq_word[i], &stated2[i], &overspeed[i], &n
xt_overspeed[i],
                &rwa_model[i], &torque[i], &power[i]);
        temp_state_2[i].position = state[i].position + coef_2 * dt * stated2[i]
posd;
        temp_state_2[i].rate = state[i].rate + coef_2 * dt * stated2[i].rated;
        temp_state_2[i].dahl = state[i].dahl + coef_2 * dt * stated2[i].dahld;

        rwa_deriv(&temp_state_2[i], torq_word[i], &stated3[i], &overspeed[i], &n
xt_overspeed[i],
                &rwa_model[i], &torque[i], &power[i]);
    }
}
```

```
temp_state_3[i].position = state[i].position + coef_3 * dt * stated3[i]
[i].posd;
temp_state_3[i].rate = state[i].rate + coef_3 * dt * stated3[i].rate
d;
temp_state_3[i].dahl = state[i].dahl + coef_3 * dt * stated3[i].dahld;

        rwa_deriv(&temp_state_3[i], torq_word[i], &stated4[i], &overspeed[i], &nxt_overspeed[i],
                &rwa_model[i], &torque[i], &power[i]);

        state[i].position += dt * (coef_4 * stated1[i].posd + coef_5 * state
d2[i].posd +
                coef_6 * stated3[i].posd + coef_7 * stated4[i].posd);
        state[i].rate += dt * (coef_4 * stated1[i].rated + coef_5 * stated2[i]
i).rated +
                coef_6 * stated3[i].rated + coef_7 * stated4[i].rated);
        state[i].dahl += dt * (coef_4 * stated1[i].dahld + coef_5 * stated2[i]
i).dahld +
                coef_6 * stated3[i].dahld + coef_7 * stated4[i].dahld);

        /* Dahl Model Friction Limiter */
        if (fabs(state[i].dahl) >= (rwa_model[i].dahl_amp))
            state[i].dahl = dsign(rwa_model[i].dahl_amp, state[i].dahl);

        /* Output Registers */

        Output(&rwa_reg[i], &rwa_model[i], &state[i], &power[i], &tach[i], &
fractional_prev_tach[i]);

        if (card[i+2].assem_write_ok != 0) {
            RWX_putbyte(&rwa_reg[i], assem_rwx[i]);
            card[i+2].assem_write_done = -1;
        };

        return 0;
    }
}
```

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rw_model.c

```
/*rw_model.c */
/* cassini itl reaction wheel model */

/* for the d_real typedef */
#include "types-darts.h"
/* for PI */
#include "generic-darts.h"

/* standard */
#include <string.h>

/* local */
#include "rw_model.h"

/* Diagnostics */
extern int model;
extern int diag_time;
extern int diag_level;
extern FILE *f_rwa;
extern int diag_flag;
extern d_real bb_tmetag;

/* namelist data */
d_real rw_num_magnets, rw_rate_est_Wn, rw_cont_Wn, rw_wheel_inertia, rw_visc_amp;
rw_dt, max_mtr_trq, trq_wrd_bits;

/* derived parameters (init) */
d_real rw_tach_scale_factor, rw_lowPassGain2, rw_lowPassGain1, rw_kp,
rw_ki, trq_scale_factor;

/* local to model */
d_real tach_t_tag_save[4], rw_rate_est[4], rw_drag_tq_est[4];
d_real old_trq_com[4];
int rwa_onoff[4], old_tach_out[4], last_pwr[4];

/** CHANGE LOG: **/
/** Modification 29 July 96 by J. Bunn:
Changed onoff to rwa_onoff to avoid conflict with other models
Changed wheel inertia to 0.16146 to match rw_params files
Changed number of magnets to 24 to match rw_params files
Added scale factor to convert from dn to torque in rw_model.c
**/

/** Modification 21 August by R. Okuno, J. Bunn, D. Garcia:
Added filter to limit tach count to max that can be expected (100 per RTI)
Added filter to limit torque command to max (0.1755)
Added filter to limit maximum drag torque
**/

/** Modification 23 August by J. Bunn, R. Okuno :
Added filter to limit tmetag to between 1 and .15 seconds
**/

/** Recent Enhancements :
1. Converted scale factor to variable calculated in rw_init (8/27/96 J. Bunn)
2. Updated rw_visc_amp to match CAB (9/27/96 J. Bunn)
3. Added code to set rate estimate to rate sample if wheels are just being turned on ( P
/27/96 J. Bunn)
**/

/** 11/22/95- Updated to have latest max motor torque
**/

void
rw_init()

int i;

/* namelist parameters */
rw_dt = 0.125;
rw_wheel_inertia = 0.15146;
rw_num_magnets = 24.;
rw_visc_amp = 1.146e-4;
rw_rate_est_Wn = 0.1; /* in Hz */
rw_cont_Wn = 0.01; /* in Hz */
max_mtr_trq = 0.17399;
trq_wrd_bits = 8;

/* derived parameters */
trq_scale_factor = max_mtr_trq / (1 << ((unsigned int)trq_wrd_bits - 1) - 1);

rw_tach_scale_factor = 2 * PI * rw_num_magnets;
rw_lowPassGain2 = exp(-(2 * PI * rw_rate_est_Wn) * rw_dt);
rw_lowPassGain1 = 1 - rw_lowPassGain2;
rw_kp = 2 * 0.707 * (2 * PI * rw_cont_Wn) * rw_wheel_inertia;
rw_ki = pow((2 * PI * rw_cont_Wn), 2) * rw_wheel_inertia;

/* initialize */
for (i = 0; i < 4; i++) {
    tach_t_tag_save[i] = 0;
    rw_rate_est[i] = 0;
    rw_drag_tq_est[i] = 0;
    old_tach_out[i] = 0;
    old_trq_com[i] = 0;
    last_pwr[i] = 0;
}

/* default wheels on */
for (i = 0; i < 4; i++)
    rwa_onoff[i] = 1;

void
rw_onoff(onoff_str)
char onoff_str[];

if (!strcmp(onoff_str, "rw1 on"))
    rwa_onoff[0] = 1;
if (!strcmp(onoff_str, "rw1 off"))
    rwa_onoff[0] = 0;
if (!strcmp(onoff_str, "rw2 on"))
    rwa_onoff[1] = 1;
if (!strcmp(onoff_str, "rw2 off"))
    rwa_onoff[1] = 0;
if (!strcmp(onoff_str, "rw3 on"))
    rwa_onoff[2] = 1;
if (!strcmp(onoff_str, "rw3 off"))
    rwa_onoff[2] = 0;
if (!strcmp(onoff_str, "rw4 on"))
    rwa_onoff[3] = 1;
if (!strcmp(onoff_str, "rw4 off"))
    rwa_onoff[3] = 0;

void
rw_model(temp_trq_com, trq_app, new_tach_out, tach_t_tag, rates, pwr_st)
d_real temp_trq_com[], trq_app[], tach_t_tag[], rates[];

int pwr_st[];
int new_tach_out[];
```

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rw_model.c

```
*
* in: temp_trq_com      commanded wheel torques tach_out      delta
* pulses tachs tach_t_tag tach read time tags rates          wheel rates
* from DARTS pwr_st     wheel power states
*
* out  trq_app          torque applied to DARTS wheels
*
{
    d_real      new_trq_com[4];
    d_real      diff_time, rate_error, corr_trq, rate_sample;
    int         i, tach_out[4];
    d_real      trq_com[4];

    /** Limiter to bound incoming trq command to +- .1755 **/

    for (i = 0; i < 4; i++) {
        /** Commanded torque comes in as dn from Bus Monitor. Needs to be
         * changed to torque. This is done via the trq_scale_factor
         **/

        new_trq_com[i] = temp_trq_com[i] * trq_scale_factor;
        if (new_trq_com[i] >= 0.0) {
            if (new_trq_com[i] > .1755)
                trq_com[i] = old_trq_com[i];
            else
                trq_com[i] = new_trq_com[i];
        } else {
            trq_com[i] = new_trq_com[i];
            if (new_trq_com[i] < -.1755)
                trq_com[i] = old_trq_com[i];
            else
                trq_com[i] = new_trq_com[i];
        }

        old_trq_com[i] = trq_com[i];

        /* Limiter to bound incoming tach data to between -100 and 100 */
        for (i = 0; i < 4; i++) {
            if (new_tach_out[i] >= 0) {
                if (new_tach_out[i] > 100)
                    tach_out[i] = old_tach_out[i];
                else
                    tach_out[i] = new_tach_out[i];
            } else
                if (new_tach_out[i] < -100)
                    tach_out[i] = old_tach_out[i];
                else
                    tach_out[i] = new_tach_out[i];

            old_tach_out[i] = tach_out[i];
        }

        for (i = 0; i < 4; i++) {
            /* if off just spin down */
            if (! (f_rwa_onoff[i] || (pwr_st[i] ||
                trq_app[i] = -rw_visc_amp * rates[i]
                last_pwr[i] = 0;
            } else {
                diff_time = tach_t_tag[i] - tach_t_tag_save[i];
                tach_t_tag_save[i] = tach_t_tag[i];
                if ((diff_time == 0.0) || (diff_time > 0.250))
                    rate_error = 0.;
            } else {
                if (diff_time < 0.10 || diff_time > 0.15)
                    diff_time = 0.125;
                /** new tach read performed - compute new rate estim
                 *
                 rate_sample = tach_out[i] * rw_tach_scale_factor / d
                 */
                if (last_pwr[i] == 0) {
                    rw_rate_est[i] = rate_sample;
                    last_pwr[i] = 1;
                } else
                    rw_rate_est[i] = rw_lowPassGain1 * rate_sample
                        + rw_lowPassGain2 * rw_rate_est[i];

                rate_error = rw_rate_est[i] - rates[i];
            }

            /* controller torque correction computation */
            corr_trq = rw_drag_tq_est[i] - rw_kp * rate_error;
            rw_drag_tq_est[i] += rw_ki * diff_time * rate_error;
            /* Limiter = 1.5(dahl_amp+visc_amp*max_speed) */
            if (rw_drag_tq_est[i] > (1.5 * (3.22e-4 + 1.146e-4 * 210)))
                rw_drag_tq_est[i] = (1.5 * (3.22e-4 + 1.146e-4 * 210)
                    + rw_drag_tq_est[i]) * .146e-4 * 210;
            if (rw_drag_tq_est[i] < -(1.5 * (3.22e-4 + 1.146e-4 * 210)))
                rw_drag_tq_est[i] = -(1.5 * (3.22e-4 + 1.146e-4 * 210)
                    + rw_drag_tq_est[i]) * .146e-4 * 210;

            trq_app[i] = trq_com[i] + corr_trq;
        }

        /* Diagnostics */

        if (model == 6 && diff_time > 0) {
            if (diag_flag == 0) {
                if ((f_rwa = fopen("/sim/tmp/rwa_diags", "w")) == (F
                    FILE *) NULL)
                    printf("File Open Failure for RWA diagnostic
                )
                diag_flag = 1;
            }
            if (diag_level == 1 || diag_level == 2 || diag_level == 3) {
                if (f_rwa == (FILE *) NULL)
                    printf("RWA %d Outputs: Torque: %5.6f \n",
                        i, trq_app[i])
                } else {
                    fprintf(f_rwa, "RWA %d Outputs: Torque: %5
                        6f \n", i, trq_app[i]
                )
            }

            if (diag_level == 2 || diag_level == 3) {
                if (f_rwa == (FILE *) NULL) {
                    t_tag %12.6f new_tach %5d rates %5.6f power %d\n" temp_trq_com[i] tach_t_tag[i]
                        , new_tach_out[i], rates[i], pwr_st[i]);
                } else {
                    fprintf(f_rwa, "
                        Inputs: temp_trq %5.6f temp_
                        t_tag[i], new_tach_out[i], rates[i], pwr_st[i]);
                }
            }

            if (diag_level == 3) {
                if (f_rwa == (FILE *) NULL) {
                    Internals t_tag_save %12.6f
                        printf."
                }
            }
        }
    }
}
```

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rw_model.c

```
rate_est %5.6f drag_tw %2.6f old_tach %5d old_torg %3.6f\n", tach_t_tag_save[i], r
w_rate_est[i], rw_drag_tw_est[i], old_tach_out[i], old_trq_com[i]);
    printf("          last_pwr %d onoff %d\n", last_pwr[i], rwa_onoff[i]);
new_trq %3.6f tach_out %5d trq_com %3.6f\n\n", last_pwr[i], rwa_onoff[i], new_trq_com[
i], tach_out[i], trq_com[i]);
    } else {
        fprintf(f_rwa, "          Internals: t_tag_save %1
2.6f rate_est %5.6f drag_tw %2.6f old_tach %5d old_torg %3.6f\n", tach_t_tag_save[i
], rw_rate_est[i], rw_drag_tw_est[i], old_tach_out[i], old_trq_com[i]);
        fprintf(f_rwa, "          last_pwr %d on
off %d new_trq %3.6f tach_out %5d trq_com %3.6f\n\n", last_pwr[i], rwa_onoff[i], new_
trq_com[i], tach_out[i], trq_com[i]);
    }

    if (model == 6) {
        if (diag_time > 0) {
            if (f_rwa == (FILE *) NULL) {
                printf("End of Cycle. bb_timetag = %f \n\n\n\n", bb_t
imetag);
                diag_time--;
            } else {
                fprintf(f_rwa, "End of Cycle. bb_timetag = %f \n\n\n\n
n", bb_timetag);
                diag_time--;
            }
        } else if (diag_time == 0) {
            diag_flag = 0;
            diag_time = -1;
            if (f_rwa != (FILE *) NULL) {
                if (fclose(f_rwa) != 0) {
                    printf("Error closing RWA Diagnostic file'\n");
                }
            }
        } else if (diag_time <= 0 && model == 6) {
            diag_time = -1;
        }
    }
}
```